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CORNELL AERONAUTICAL LABORATORY, INC.

Report No. BE-1007-A-5

THERMODYNAMIC PROPERTIES OF NITROGEN
FROM 2000°K TO 8000°K

BY

C. E. Treanor and J. O. Logan, Jr.

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B U F F A L O , N E W Y O R K

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F.K. Moore, Head
Aerodynamic Research Dept.

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ABSTRACT

~~This report presents~~ [↓] tables of thermodynamic properties of nitrogen at high temperatures, including effects of dissociation and ionization. The partition functions, first and second temperature derivatives of partition functions, equilibrium constants and temperature derivatives of equilibrium constants are tabulated at intervals of 500°K between 2000°K and 8000°K. The mole fraction composition, temperature and density derivatives of mole fraction composition, pressure, entropy, enthalpy, specific heats and speed of sound are tabulated at the temperatures given above and at densities of ^{1/1000, 1/100, 1/10} ~~10⁻³, 10⁻², 10⁻¹~~, 1 and 10 times standard atmospheric density. All quantities were calculated directly from the formulas of statistical mechanics, using digital computers and employing the most recent spectroscopic data. Effects of the second virial coefficient are not included. [↙]

TABLE OF CONTENTS

	<u>Page</u>
LIST OF SYMBOLS	iii
INTRODUCTION.	1
NUMERICAL CALCULATIONS.	1
LIST AND DESCRIPTION OF TABLES.	2
REFERENCES.	4
ACKNOWLEDGEMENTS.	5

LIST OF SYMBOLS

a	Speed of sound
c_p	Specific heat at constant pressure
c_v	Specific heat at constant volume
f_1	Partition function, including translation, dissociation and ionization for species 1
H	Enthalpy
K_1, K_2, K_3	Equilibrium constants (see "Contents of Tables", Table IV)
M	Molecular weight of gas
M_1	Molecular weight of 1 th species
$[N_2], [N]$ etc.	Number of moles of N_2 , N , etc. originating from one mole of N_2 at standard conditions
P	Pressure
Q_1	Internal partition functions for species 1
S	Entropy
T	Temperature ($^{\circ}K$)
X_1	Mole fraction of species 1, i.e., number of moles of species 1 per mole of gas
Z	Total number of moles of gas originating from one mole of N_2 at standard conditions
γ	Specific heat ratio
ρ	Density

Subscript zero refers to NACA standard conditions (see page 2)

INTRODUCTION

In the course of calculating the thermodynamic properties of air at high temperatures¹, the partition functions for the atomic and molecular constituents of air were calculated from spectroscopic data and were available on punched cards. A relatively easy program could then be prepared for the IBM card programmed calculator to obtain the thermodynamic properties of pure oxygen and pure nitrogen. Tables of these properties are of value in various aerodynamic calculations, and are not available at present in a form that includes the effects of dissociation and ionization. Accordingly, the calculations were performed for oxygen over the temperature range from 2000°K to 5000°K at 100° intervals and for 15 densities between 10^{-3} and about 15 times standard atmospheric density². The present report is the result of a similar calculation for nitrogen covering the temperature range from 2000°K to 8000°K at 500° intervals and for five densities from 10^{-3} to 10 times atmospheric density.

NUMERICAL CALCULATIONS

The thermodynamic properties of nitrogen that are tabulated herein were calculated from spectroscopic data as given in Herzberg³ and Moore⁴, with the exception that the dissociation energy of N_2 was taken as 9.756 e.v. instead of the value given in Herzberg. The formulas and calculation procedures that were used are exactly parallel to those used for oxygen in Ref. 2, and so are not repeated here. All calculations were performed on the IBM card-programmed calculator at Cornell Aeronautical Laboratory. Reference conditions (subscript zero) were taken at the pressure and

temperature of NACA standard reference conditions in order to make the tables most useful for aerodynamic calculations. These conditions are

$$P_0 = 1.013 \times 10^6 \frac{\text{dynes}}{\text{cm}^2} = 14.7 \frac{\text{lbs.}}{\text{in.}^2} \quad T_0 = 288.10^\circ\text{K} = 518.6^\circ\text{R}$$

Thus, with the molecular weight of $N_2 = 28.014$ and $\gamma_0 = 1.4$,

$$\rho_0 = 1.1845 \times 10^{-3} \frac{\text{gms}}{\text{cm}^3} = 2.2963 \times 10^{-4} \frac{\text{slug}}{\text{ft}^3}$$

$$a_0 = 3.460 \times 10^4 \frac{\text{cm}}{\text{sec.}} = 1135 \frac{\text{ft.}}{\text{sec.}}$$

It should be pointed out that these reference conditions are different from those used by Woolley⁵ in his calculations for undissociated nitrogen. Also the present calculations do not include the real gas effects of the higher virial coefficients, which are included in Woolley's work.

LIST AND DESCRIPTION OF TABLES

The temperature range covered in the tables is 2000°K to 8000°K at intervals of 500°K . The functions which are density dependent were calculated at density values of $\rho/\rho_0 = 10^{-3}, 10^{-2}, 10^{-1}, 1$ and 10 . Tables I through IX contain functions which are not density dependent. These are:

Table I Internal partition functions Q_i

Table II Temperature derivatives of partition functions, $\frac{dQ_i}{dT}$

Table III Second temperature derivatives of partition functions, $\frac{d^2Q_i}{dT^2}$

Table IV $\frac{\rho}{\rho_0}$ times the equilibrium constants

$$K_1 = \frac{[N]^2}{[N_2]} \quad K_2 = \frac{[N_2^+][e^-]}{[N_2]} \quad K_3 = \frac{[N^+][e^-]}{[N]}$$

Table V	Temperature derivatives of the \ln of the equilibrium constant from Table IV
Table VI	P/P_0 times the partition functions including translation, dissociation and ionization
Table VII	\ln of partition functions from Table VI
Table VIII	Temperature derivatives of \ln of the partition functions from Table VI
Table IX	Temperature derivatives of the product of T^2 and temperature derivatives from Table VIII

The remaining tables list functions which are density dependent:

Table X	Mole fractions, the fractional number of particles of each species at a given temperature and density
Table XI	Temperature derivatives of mole fractions from Table X (density const.)
Table XII	Density derivatives of mole fractions from Table X (temp. const.)
Table XIII	Entropy in non-dimensional form and in cal/gm ^o K; enthalpy in non-dimensional form and in cal/gm; compressibility factor Z, equal to the ratio of the molecular weight at standard conditions to the molecular weight
Table XIV	Pressure P/P_0 ; density derivatives of P/P_0 at constant temperature; gram molecular weight; and derivatives of the molecular weight with respect to temperature and density.
Table XV	Specific heat at constant volume; specific heat at constant pressure; specific heat ratio $\gamma = c_p/c_v$; and speed of sound a/a_0 .

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T°K	Q_{N_2}	Q_N	$Q_{N_2^+}$	Q_{N^+}
2000	8.57628X10 ⁻⁰²	4.00000X10 ⁻⁰⁰	1.84392X10 ⁻⁰³	8.44543X10 ⁻⁰⁰
2500	1.18249X10 ⁻⁰³	4.00015X10 ⁻⁰⁰	2.58307X10 ⁻⁰³	8.55336X10 ⁻⁰⁰
3000	1.56062X10 ⁻⁰³	4.00099X10 ⁻⁰⁰	3.48782X10 ⁻⁰³	8.62835X10 ⁻⁰⁰
3500	1.99280X10 ⁻⁰³	4.00374X10 ⁻⁰⁰	4.59028X10 ⁻⁰³	8.68664X10 ⁻⁰⁰
4000	2.47969X10 ⁻⁰³	4.01012X10 ⁻⁰⁰	5.92312X10 ⁻⁰³	8.73718X10 ⁻⁰⁰
4500	3.02183X10 ⁻⁰³	4.02202X10 ⁻⁰⁰	7.51740X10 ⁻⁰³	8.78519X10 ⁻⁰⁰
5000	3.61975X10 ⁻⁰³	4.04111X10 ⁻⁰⁰	9.40179X10 ⁻⁰³	8.83367X10 ⁻⁰⁰
5500	4.27399X10 ⁻⁰³	4.06867X10 ⁻⁰⁰	1.16024X10 ⁻⁰⁴	8.88422X10 ⁻⁰⁰
6000	4.98513X10 ⁻⁰³	4.10555X10 ⁻⁰⁰	1.41430X10 ⁻⁰⁴	8.93756X10 ⁻⁰⁰
6500	5.75386X10 ⁻⁰³	4.15212X10 ⁻⁰⁰	1.70456X10 ⁻⁰⁴	8.99391X10 ⁻⁰⁰
7000	6.58108X10 ⁻⁰³	4.20840X10 ⁻⁰⁰	2.03301X10 ⁻⁰⁴	9.05315X10 ⁻⁰⁰
7500	7.46802X10 ⁻⁰³	4.27413X10 ⁻⁰⁰	2.40153X10 ⁻⁰⁴	9.11503X10 ⁻⁰⁰
8000	8.41640X10 ⁻⁰³	4.34884X10 ⁻⁰⁰	2.81188X10 ⁻⁰⁴	9.17923X10 ⁻⁰⁰

Table I

Internal partition functions

T°K	$\frac{dQ_{N_2}}{dT}$	$\frac{dQ_N}{dT}$	$\frac{dQ_{N_2^+}}{dT}$	$\frac{dQ_{N^+}}{dT}$
2000	5.97216X10 ⁻⁰¹	6.83546X10 ⁻⁰⁸	1.33239X10 ⁻⁰⁰	2.66394X10 ⁻⁰⁴
2500	7.02669X10 ⁻⁰¹	6.96904X10 ⁻⁰⁷	1.63362X10 ⁻⁰⁰	1.75680X10 ⁻⁰⁴
3000	8.10084X10 ⁻⁰¹	3.07505X10 ⁻⁰⁶	1.99621X10 ⁻⁰⁰	1.29435X10 ⁻⁰⁴
3500	9.18882X10 ⁻⁰¹	8.50111X10 ⁻⁰⁶	2.42458X10 ⁻⁰⁰	1.06599X10 ⁻⁰⁴
4000	1.02884X10 ⁻⁰⁰	1.76660X10 ⁻⁰⁵	2.91714X10 ⁻⁰⁰	9.72546X10 ⁻⁰⁵
4500	1.13988X10 ⁻⁰⁰	3.04816X10 ⁻⁰⁵	3.46955X10 ⁻⁰⁰	9.57709X10 ⁻⁰⁵
5000	1.25198X10 ⁻⁰⁰	4.63053X10 ⁻⁰⁵	4.07670X10 ⁻⁰⁰	9.86669X10 ⁻⁰⁵
5500	1.36517X10 ⁻⁰⁰	6.42430X10 ⁻⁰⁵	4.73370X10 ⁻⁰⁰	1.03753X10 ⁻⁰⁴
6000	1.47961X10 ⁻⁰⁰	8.33773X10 ⁻⁰⁵	5.43623X10 ⁻⁰⁰	1.09682X10 ⁻⁰⁴
6500	1.59560X10 ⁻⁰⁰	1.02895X10 ⁻⁰⁴	6.18062X10 ⁻⁰⁰	1.15653X10 ⁻⁰⁴
7000	1.71367X10 ⁻⁰⁰	1.22142X10 ⁻⁰⁴	6.96375X10 ⁻⁰⁰	1.21228X10 ⁻⁰⁴
7500	1.83463X10 ⁻⁰⁰	1.40628X10 ⁻⁰⁴	7.78302X10 ⁻⁰⁰	1.26189X10 ⁻⁰⁴
8000	1.95966X10 ⁻⁰⁰	1.58013X10 ⁻⁰⁴	8.63626X10 ⁻⁰⁰	1.30460X10 ⁻⁰⁴

Table II

Temperature derivatives of partition functions

T°K	$\frac{d^2 Q_M}{dT^2}$	$\frac{d^2 Q_M}{dT^2}$	$\frac{d^2 Q_M}{dT^2}$
2000	2.08136X10 ⁻⁰⁴	4.04453X10 ⁻¹⁰	5.48202X10 ⁻⁰⁴
2500	2.13166X10 ⁻⁰⁴	2.53168X10 ⁻⁰⁹	6.61011X10 ⁻⁰⁴
3000	2.16320X10 ⁻⁰⁴	7.44109X10 ⁻⁰⁹	7.90735X10 ⁻⁰⁴
3500	2.18805X10 ⁻⁰⁴	1.44976X10 ⁻⁰⁸	9.22094X10 ⁻⁰⁴
4000	2.21020X10 ⁻⁰⁴	2.21235X10 ⁻⁰⁸	1.04663X10 ⁻⁰³
4500	2.23132X10 ⁻⁰⁴	2.89141X10 ⁻⁰⁸	1.16125X10 ⁻⁰³
5000	2.25260X10 ⁻⁰⁴	3.40749X10 ⁻⁰⁸	1.26569X10 ⁻⁰³
5500	2.27563X10 ⁻⁰⁴	3.73659X10 ⁻⁰⁸	1.36086X10 ⁻⁰³
6000	2.30296X10 ⁻⁰⁴	3.88986X10 ⁻⁰⁸	1.44804X10 ⁻⁰³
6500	2.33838X10 ⁻⁰⁴	3.89553X10 ⁻⁰⁸	1.52846X10 ⁻⁰³
7000	2.38706X10 ⁻⁰⁴	3.78695X10 ⁻⁰⁸	1.60320X10 ⁻⁰³
7500	2.45540X10 ⁻⁰⁴	3.59615X10 ⁻⁰⁸	1.67318X10 ⁻⁰³
8000	2.55075X10 ⁻⁰⁴	3.35094X10 ⁻⁰⁸	1.73915X10 ⁻⁰³

Table III

Second temperature derivatives
of partition functions

T°K	% K ₁	% K ₂	% K ₃
2000	1.20430X10 ⁻¹⁹	2.09937X10 ⁻³⁸	8.40159X10 ⁻³⁶
2500	1.00389X10 ⁻¹⁴	2.09706X10 ⁻³⁰	2.51453X10 ⁻²⁸
3000	1.89170X10 ⁻¹¹	4.80632X10 ⁻²⁵	2.54928X10 ⁻²³
3500	4.09453X10 ⁻⁰⁹	3.40518X10 ⁻²¹	9.94647X10 ⁻²⁰
4000	2.29626X10 ⁻⁰⁷	2.73842X10 ⁻¹⁸	5.04242X10 ⁻¹⁷
4500	5.24498X10 ⁻⁰⁶	5.14838X10 ⁻¹⁶	6.53504X10 ⁻¹⁵
5000	6.40205X10 ⁻⁰⁵	3.49041X10 ⁻¹⁴	3.25122X10 ⁻¹³
5500	4.96370X10 ⁻⁰⁴	1.12440X10 ⁻¹²	8.04493X10 ⁻¹²
6000	2.74276X10 ⁻⁰³	2.06889X10 ⁻¹¹	1.17698X10 ⁻¹⁰
6500	1.16944X10 ⁻⁰²	2.47017X10 ⁻¹⁰	1.14782X10 ⁻⁰⁹
7000	4.07127X10 ⁻⁰²	2.09667X10 ⁻⁰⁹	8.13071X10 ⁻⁰⁹
7500	1.20595X10 ⁻⁰¹	1.35292X10 ⁻⁰⁸	4.45596X10 ⁻⁰⁸
8000	3.13395X10 ⁻⁰¹	6.97980X10 ⁻⁰⁸	1.98126X10 ⁻⁰⁷

Table IV

$\frac{p}{e}$ times the equilibrium constants

$T^{\circ}K$	$\frac{1}{K_1} \frac{\partial K_1}{\partial T}$	$\frac{1}{K_2} \frac{\partial K_2}{\partial T}$	$\frac{1}{K_3} \frac{\partial K_3}{\partial T}$
2000	2.83470X10 ⁻⁰²	4.59481X10 ⁻⁰²	4.29489X10 ⁻⁰²
2500	1.81138X10 ⁻⁰²	2.95482X10 ⁻⁰²	2.76075X10 ⁻⁰²
3000	1.25572X10 ⁻⁰²	2.06256X10 ⁻⁰²	1.92553X10 ⁻⁰²
3500	9.21036X10 ⁻⁰³	1.52456X10 ⁻⁰²	1.42076X10 ⁻⁰²
4000	7.04224X10 ⁻⁰³	1.17455X10 ⁻⁰²	1.09233X10 ⁻⁰²
4500	5.56008X10 ⁻⁰³	9.34050X10 ⁻⁰³	8.66602X10 ⁻⁰³
5000	4.50397X10 ⁻⁰³	7.61524X10 ⁻⁰³	7.04649X10 ⁻⁰³
5500	3.72616X10 ⁻⁰³	6.33445X10 ⁻⁰³	5.84447X10 ⁻⁰³
6000	3.13751X10 ⁻⁰³	5.35667X10 ⁻⁰³	4.92723X10 ⁻⁰³
6500	2.68168X10 ⁻⁰³	4.59268X10 ⁻⁰³	4.21102X10 ⁻⁰³
7000	2.32160X10 ⁻⁰³	3.98392X10 ⁻⁰³	3.64089X10 ⁻⁰³
7500	2.03211X10 ⁻⁰³	3.49064X10 ⁻⁰³	3.17951X10 ⁻⁰³
8000	1.79566X10 ⁻⁰³	3.08504X10 ⁻⁰³	2.80084X10 ⁻⁰³

Table V

Temperature derivatives of \ln
of equilibrium constants

$T^{\circ}K$	$\% f_{N_2}^{+34}$	$\% f_N^{+19}$	$\% f_{N_2}^{+05}$	$\% f_{N^+}^{+17}$	$\% f_{e^-}^{+25}$
2000	2.52884X10 ⁺³⁴	4.30054X10 ⁺¹⁹	3.15886X10 ⁺⁰⁵	2.14745X10 ⁺¹⁷	1.02176X10 ⁺²⁵
2500	4.87291X10 ⁺³⁴	1.72359X10 ⁺²²	4.34967X10 ⁺⁰³	1.84317X10 ⁺⁰⁷	1.42795X10 ⁺²⁵
3000	8.45390X10 ⁺³⁴	9.85485X10 ⁺²³	1.31550X10 ⁺⁰⁹	8.12773X10 ⁺⁰¹	1.87709X10 ⁺²⁵
3500	1.36033X10 ⁺³⁵	1.83916X10 ⁺²⁵	1.18998X10 ⁺¹³	4.69647X10 ⁺⁰⁴	2.36541X10 ⁺²⁵
4000	2.06807X10 ⁺³⁵	1.69819X10 ⁺²⁶	1.19069X10 ⁺¹⁶	1.79937X10 ⁺⁰⁸	2.88998X10 ⁺²⁵
4500	3.00723X10 ⁺³⁵	9.78703X10 ⁺²⁶	2.72782X10 ⁺¹⁸	1.12632X10 ⁺¹¹	3.44845X10 ⁺²⁵
5000	4.21903X10 ⁺³⁵	4.05005X10 ⁺²⁷	2.21518X10 ⁺²⁰	1.97987X10 ⁺¹³	4.03887X10 ⁺²⁵
5500	5.74720X10 ⁺³⁵	1.31621X10 ⁺²⁸	8.42547X10 ⁺²¹	1.38003X10 ⁺¹⁵	4.65960X10 ⁺²⁵
6000	7.63805X10 ⁺³⁵	3.56681X10 ⁺²⁸	1.80816X10 ⁺²³	4.80184X10 ⁺¹⁶	5.30923X10 ⁺²⁵
6500	9.94050X10 ⁺³⁵	8.40212X10 ⁺²⁸	2.49170X10 ⁺²⁴	9.78318X10 ⁺¹⁷	5.98653X10 ⁺²⁵
7000	1.27064X10 ⁺³⁶	1.77244X10 ⁺²⁹	2.41895X10 ⁺²⁵	1.30808X10 ⁺¹⁹	6.69040X10 ⁺²⁵
7500	1.59910X10 ⁺³⁶	3.42214X10 ⁺²⁹	1.77121X10 ⁺²⁶	1.24805X10 ⁺²⁰	7.41988X10 ⁺²⁵
8000	1.98536X10 ⁺³⁶	6.14697X10 ⁺²⁹	1.02979X10 ⁺²⁷	9.04801X10 ⁺²⁰	8.17410X10 ⁺²⁵

Table VI

$\% f$ times partition functions

T°K	$\ln \rho / \rho_0 f_{N_2}$	$\ln \rho / \rho_0 f_N$	$\ln \rho / \rho_0 f_{N_2^+}$	$\ln \rho / \rho_0 f_{N^+}$	$\ln \rho / \rho_0 f_{e^-}$
2000	7.92156X10 ⁻⁰¹	4.52078X10 ⁻⁰¹	-1.03627X10 ⁻⁰¹	-3.83796X10 ⁻⁰¹	5.75861X10 ⁻⁰¹
2500	7.98715X10 ⁻⁰¹	5.12012X10 ⁻⁰¹	8.37785X10 ⁻⁰⁰	-1.55066X10 ⁻⁰¹	5.79208X10 ⁻⁰¹
3000	8.04225X10 ⁻⁰¹	5.52474X10 ⁻⁰¹	2.09974X10 ⁻⁰¹	-2.07302X10 ⁻⁰¹	5.81943X10 ⁻⁰¹
3500	8.08982X10 ⁻⁰¹	5.81739X10 ⁻⁰¹	3.01075X10 ⁻⁰¹	1.07571X10 ⁻⁰¹	5.84255X10 ⁻⁰¹
4000	8.13170X10 ⁻⁰¹	6.03967X10 ⁻⁰¹	3.70159X10 ⁻⁰¹	1.90081X10 ⁻⁰¹	5.86258X10 ⁻⁰¹
4500	8.16915X10 ⁻⁰¹	6.21482X10 ⁻⁰¹	4.24500X10 ⁻⁰¹	2.54473X10 ⁻⁰¹	5.88025X10 ⁻⁰¹
5000	8.20300X10 ⁻⁰¹	6.35685X10 ⁻⁰¹	4.68470X10 ⁻⁰¹	3.06166X10 ⁻⁰¹	5.89605X10 ⁻⁰¹
5500	8.23391X10 ⁻⁰¹	6.47471X10 ⁻⁰¹	5.04855X10 ⁻⁰¹	3.48608X10 ⁻⁰¹	5.91035X10 ⁻⁰¹
6000	8.26236X10 ⁻⁰¹	6.57440X10 ⁻⁰¹	5.35517X10 ⁻⁰¹	3.84103X10 ⁻⁰¹	5.92340X10 ⁻⁰¹
6500	8.28870X10 ⁻⁰¹	6.66008X10 ⁻⁰¹	5.61750X10 ⁻⁰¹	4.14246X10 ⁻⁰¹	5.93541X10 ⁻⁰¹
7000	8.31325X10 ⁻⁰¹	6.73473X10 ⁻⁰¹	5.84479X10 ⁻⁰¹	4.40176X10 ⁻⁰¹	5.94653X10 ⁻⁰¹
7500	8.33625X10 ⁻⁰¹	6.80052X10 ⁻⁰¹	6.04388X10 ⁻⁰¹	4.62732X10 ⁻⁰¹	5.95687X10 ⁻⁰¹
8000	8.35788X10 ⁻⁰¹	6.85909X10 ⁻⁰¹	6.21991X10 ⁻⁰¹	4.82542X10 ⁻⁰¹	5.96655X10 ⁻⁰¹

Table VII

 \ln of partition functions

T°K	$\frac{\partial}{\partial T} \ln f_{N_2}$	$\frac{\partial}{\partial T} \ln f_N$	$\frac{\partial}{\partial T} \ln f_{N_2^+}$	$\frac{\partial}{\partial T} \ln f_{N^+}$	$\frac{\partial}{\partial T} \ln f_{e^-}$
2000	1.44635X10 ⁻⁰³	1.48966X10 ⁻⁰²	4.66445X10 ⁻⁰²	5.70956X10 ⁻⁰²	7.50000X10 ⁻⁰⁴
2500	1.19422X10 ⁻⁰³	9.65404X10 ⁻⁰³	3.01424X10 ⁻⁰²	3.66615X10 ⁻⁰²	6.00000X10 ⁻⁰⁴
3000	1.01907X10 ⁻⁰³	6.78817X10 ⁻⁰³	2.11487X10 ⁻⁰²	2.55434X10 ⁻⁰²	5.00000X10 ⁻⁰⁴
3500	8.89670X10 ⁻⁰⁴	5.05001X10 ⁻⁰³	1.57067X10 ⁻⁰²	1.88291X10 ⁻⁰²	4.28571X10 ⁻⁰⁴
4000	7.89908X10 ⁻⁰⁴	3.91607X10 ⁻⁰³	1.21604X10 ⁻⁰²	1.44646X10 ⁻⁰²	3.75000X10 ⁻⁰⁴
4500	7.10549X10 ⁻⁰⁴	3.13531X10 ⁻⁰³	9.71771X10 ⁻⁰³	1.14680X10 ⁻⁰²	3.33333X10 ⁻⁰⁴
5000	6.45874X10 ⁻⁰⁴	2.57492X10 ⁻⁰³	7.96111X10 ⁻⁰³	9.32142X10 ⁻⁰³	3.00000X10 ⁻⁰⁴
5500	5.92141X10 ⁻⁰⁴	2.15915X10 ⁻⁰³	6.65386X10 ⁻⁰³	7.73089X10 ⁻⁰³	2.72727X10 ⁻⁰⁴
6000	5.46805X10 ⁻⁰⁴	1.84216X10 ⁻⁰³	5.65347X10 ⁻⁰³	6.51939X10 ⁻⁰³	2.50000X10 ⁻⁰⁴
6500	5.08079X10 ⁻⁰⁴	1.59488X10 ⁻⁰³	4.86999X10 ⁻⁰³	5.57514X10 ⁻⁰³	2.30769X10 ⁻⁰⁴
7000	4.74679X10 ⁻⁰⁴	1.39813X10 ⁻⁰³	4.24432X10 ⁻⁰³	4.82474X10 ⁻⁰³	2.14285X10 ⁻⁰⁴
7500	4.45665X10 ⁻⁰⁴	1.23888X10 ⁻⁰³	3.73631X10 ⁻⁰³	4.21840X10 ⁻⁰³	2.00000X10 ⁻⁰⁴
8000	4.20338X10 ⁻⁰⁴	1.10800X10 ⁻⁰³	3.31787X10 ⁻⁰³	3.72134X10 ⁻⁰³	1.87500X10 ⁻⁰⁴

Table VIII

Temperature derivatives of \ln
of partition functions

$T^{\circ}K$	$\frac{\partial}{\partial T} T^2 \frac{\partial}{\partial T} \ln f_{N_2}$	$\frac{\partial}{\partial T} T^2 \frac{\partial}{\partial T} \ln f_N$	$\frac{\partial}{\partial T} T^2 \frac{\partial}{\partial T} \ln f_{N_2^+}$	$\frac{\partial}{\partial T} T^2 \frac{\partial}{\partial T} \ln f_{N^+}$	$\frac{\partial}{\partial T} T^2 \frac{\partial}{\partial T} \ln f_e$
2000	3.31652X10 ⁺⁰⁰	1.50047X10 ⁺⁰⁰	3.49102X10 ⁺⁰⁰	1.74195X10 ⁺⁰⁰	1.50000X10 ⁺⁰⁰
2500	3.39090X10 ⁺⁰⁰	1.50482X10 ⁺⁰⁰	3.76172X10 ⁺⁰⁰	1.69263X10 ⁺⁰⁰	1.50000X10 ⁺⁰⁰
3000	3.43699X10 ⁺⁰⁰	1.52134X10 ⁺⁰⁰	4.02630X10 ⁺⁰⁰	1.52053X10 ⁺⁰⁰	1.50000X10 ⁺⁰⁰
3500	3.46821X10 ⁺⁰⁰	1.55916X10 ⁺⁰⁰	4.24048X10 ⁺⁰⁰	1.54202X10 ⁺⁰⁰	1.50000X10 ⁺⁰⁰
4000	3.49100X10 ⁺⁰⁰	1.62320X10 ⁺⁰⁰	4.38634X10 ⁺⁰⁰	1.56987X10 ⁺⁰⁰	1.50000X10 ⁺⁰⁰
4500	3.50878X10 ⁺⁰⁰	1.71262X10 ⁺⁰⁰	4.46839X10 ⁺⁰⁰	1.60105X10 ⁺⁰⁰	1.50000X10 ⁺⁰⁰
5000	3.52378X10 ⁺⁰⁰	1.82210X10 ⁺⁰⁰	4.50123X10 ⁺⁰⁰	1.63277X10 ⁺⁰⁰	1.50000X10 ⁺⁰⁰
5500	3.53791X10 ⁺⁰⁰	1.94395X10 ⁺⁰⁰	4.50063X10 ⁺⁰⁰	1.66300X10 ⁺⁰⁰	1.50000X10 ⁺⁰⁰
6000	3.55337X10 ⁺⁰⁰	2.06994X10 ⁺⁰⁰	4.47959X10 ⁺⁰⁰	1.69056X10 ⁺⁰⁰	1.50000X10 ⁺⁰⁰
6500	3.57301X10 ⁺⁰⁰	2.19260X10 ⁺⁰⁰	4.44745X10 ⁺⁰⁰	1.71490X10 ⁺⁰⁰	1.50000X10 ⁺⁰⁰
7000	3.60038X10 ⁺⁰⁰	2.30598X10 ⁺⁰⁰	4.41040X10 ⁺⁰⁰	1.73594X10 ⁺⁰⁰	1.50000X10 ⁺⁰⁰
7500	3.63964X10 ⁺⁰⁰	2.40591X10 ⁺⁰⁰	4.37228X10 ⁺⁰⁰	1.75391X10 ⁺⁰⁰	1.50000X10 ⁺⁰⁰
8000	3.69537X10 ⁺⁰⁰	2.49000X10 ⁺⁰⁰	4.33533X10 ⁺⁰⁰	1.76915X10 ⁺⁰⁰	1.50000X10 ⁺⁰⁰

Table IX Temperature derivatives of the product of T^2 and temperature derivatives of \ln of partition functions

T°K	X _{N₂}	X _N	X _{N₂⁺}	X _{N⁺}	X _{e⁻}
2000	1.00000X10 ⁻⁰⁰	1.09740X10 ⁻⁰⁸	4.58188X10 ⁻¹⁸	2.01225X10 ⁻²³	4.58190X10 ⁻¹⁸
2500	9.99996X10 ⁻⁰¹	3.16842X10 ⁻⁰⁶	4.57848X10 ⁻¹⁴	1.73945X10 ⁻¹⁷	4.58022X10 ⁻¹⁴
3000	9.99862X10 ⁻⁰¹	1.37524X10 ⁻⁰⁴	2.18415X10 ⁻¹¹	1.59341X10 ⁻¹³	2.20008X10 ⁻¹¹
3500	9.97979X10 ⁻⁰¹	2.02042X10 ⁻⁰³	1.79034X10 ⁻⁰⁹	1.05873X10 ⁻¹⁰	1.89621X10 ⁻⁰⁹
4000	9.85016X10 ⁻⁰¹	1.49830X10 ⁻⁰²	4.57319X10 ⁻⁰⁸	1.28089X10 ⁻⁰⁸	5.85409X10 ⁻⁰⁸
4500	9.31317X10 ⁻⁰¹	6.86804X10 ⁻⁰²	4.89028X10 ⁻⁰⁷	4.57769X10 ⁻⁰⁷	9.46798X10 ⁻⁰⁷
5000	7.87675X10 ⁻⁰¹	2.12305X10 ⁻⁰¹	2.64573X10 ⁻⁰⁶	6.64251X10 ⁻⁰⁶	9.28825X10 ⁻⁰⁶
5500	5.43565X10 ⁻⁰¹	4.56319X10 ⁻⁰¹	8.20502X10 ⁻⁰⁶	4.92828X10 ⁻⁰⁵	5.74879X10 ⁻⁰⁵
6000	2.87342X10 ⁻⁰¹	7.12177X10 ⁻⁰¹	1.59174X10 ⁻⁰⁵	2.24437X10 ⁻⁰⁴	2.640354X10 ⁻⁰⁴
6500	1.18484X10 ⁻⁰¹	8.79990X10 ⁻⁰¹	2.14618X10 ⁻⁰⁵	7.40680X10 ⁻⁰⁴	7.62142X10 ⁻⁰⁴
7000	4.28713X10 ⁻⁰²	9.53088X10 ⁻⁰¹	2.31604X10 ⁻⁰⁵	1.99669X10 ⁻⁰³	2.01985X10 ⁻⁰³
7500	1.55955X10 ⁻⁰²	9.75009X10 ⁻⁰¹	2.27033X10 ⁻⁰⁵	4.67484X10 ⁻⁰³	4.69754X10 ⁻⁰³
8000	6.08031X10 ⁻⁰³	9.74286X10 ⁻⁰¹	2.15355X10 ⁻⁰⁵	9.79523X10 ⁻⁰³	9.81676X10 ⁻⁰³

log P/P₀ = -3.0

T°K	X _{N₂}	X _N	X _{N₂⁺}	X _{N⁺}	X _{e⁻}
2000	1.00000X10 ⁻⁰⁰	3.47030X10 ⁻⁰⁹	1.44892X10 ⁻¹⁸	2.01225X10 ⁻²⁴	1.44892X10 ⁻¹⁸
2500	9.99999X10 ⁻⁰¹	1.00194X10 ⁻⁰⁶	1.44803X10 ⁻¹⁴	1.73968X10 ⁻¹⁸	1.44821X10 ⁻¹⁴
3000	9.99956X10 ⁻⁰¹	4.34922X10 ⁻⁰⁵	6.92455X10 ⁻¹²	1.59745X10 ⁻¹⁴	6.94052X10 ⁻¹²
3500	9.99360X10 ⁻⁰¹	6.39578X10 ⁻⁰⁴	5.77883X10 ⁻¹⁰	1.08028X10 ⁻¹¹	5.88686X10 ⁻¹⁰
4000	9.95225X10 ⁻⁰¹	4.77476X10 ⁻⁰³	1.58055X10 ⁻⁰⁸	1.39629X10 ⁻⁰⁹	1.72018X10 ⁻⁰⁸
4500	9.77484X10 ⁻⁰¹	2.25148X10 ⁻⁰²	1.96217X10 ⁻⁰⁷	5.73686X10 ⁻⁰⁸	2.53586X10 ⁻⁰⁷
5000	9.24526X10 ⁻⁰¹	7.54686X10 ⁻⁰²	1.32814X10 ⁻⁰⁶	1.00986X10 ⁻⁰⁶	2.33800X10 ⁻⁰⁶
5500	8.09332X10 ⁻⁰¹	1.90638X10 ⁻⁰¹	5.53695X10 ⁻⁰⁶	9.33151X10 ⁻⁰⁶	1.48684X10 ⁻⁰⁵
6000	6.26178X10 ⁻⁰¹	3.73684X10 ⁻⁰¹	1.54810X10 ⁻⁰⁵	5.25581X10 ⁻⁰⁵	6.80392X10 ⁻⁰⁵
6500	4.14268X10 ⁻⁰¹	5.85263X10 ⁻⁰¹	3.09262X10 ⁻⁰⁵	2.03023X10 ⁻⁰⁴	2.33949X10 ⁻⁰⁴
7000	2.33394X10 ⁻⁰¹	7.65318X10 ⁻⁰¹	4.68952X10 ⁻⁰⁵	5.96318X10 ⁻⁰⁴	6.43213X10 ⁻⁰⁴
7500	1.15624X10 ⁻⁰¹	8.81358X10 ⁻⁰¹	5.77775X10 ⁻⁰⁵	1.45053X10 ⁻⁰³	1.50830X10 ⁻⁰³
8000	5.36748X10 ⁻⁰²	9.40006X10 ⁻⁰¹	6.22947X10 ⁻⁰⁵	3.09678X10 ⁻⁰³	3.15908X10 ⁻⁰³

log P/P₀ = -2.0

Table X Mole Fractions

T°K	X_{N_2}	X_N	$X_{N_2^+}$	X_{N^+}	X_{e^-}
2000	1.00000X10 ⁺⁰⁰	1.09740X10 ⁻⁰⁹	4.58189X10 ⁻¹⁹	2.01225X10 ⁻²⁵	4.58189X10 ⁻¹⁹
2500	9.99999X10 ⁻⁰¹	3.16843X10 ⁻⁰⁷	4.57928X10 ⁻¹⁵	1.73975X10 ⁻¹⁹	4.57945X10 ⁻¹⁵
3000	9.99986X10 ⁻⁰¹	1.37537X10 ⁻⁰⁵	2.19151X10 ⁻¹²	1.59873X10 ⁻¹⁵	2.19310X10 ⁻¹²
3500	9.99797X10 ⁻⁰¹	2.02318X10 ⁻⁰⁴	1.83960X10 ⁻¹⁰	1.08736X10 ⁻¹²	1.85048X10 ⁻¹⁰
4000	9.98486X10 ⁻⁰¹	1.51362X10 ⁻⁰³	5.15559X10 ⁻⁰⁹	1.43910X10 ⁻¹⁰	5.29950X10 ⁻⁰⁹
4500	9.92796X10 ⁻⁰¹	7.20309X10 ⁻⁰³	6.82891X10 ⁻⁰⁸	6.28909X10 ⁻⁰⁹	7.45782X10 ⁻⁰⁸
5000	9.75168X10 ⁻⁰¹	2.48305X10 ⁻⁰²	5.21253X10 ⁻⁰⁷	1.23630X10 ⁻⁰⁷	6.44884X10 ⁻⁰⁷
5500	9.33084X10 ⁻⁰¹	6.69073X10 ⁻⁰²	2.58885X10 ⁻⁰⁶	1.32818X10 ⁻⁰⁶	3.91703X10 ⁻⁰⁶
6000	8.52765X10 ⁻⁰¹	1.47198X10 ⁻⁰¹	9.08088X10 ⁻⁰⁶	8.91729X10 ⁻⁰⁶	1.79981X10 ⁻⁰⁵
6500	7.28520X10 ⁻⁰¹	2.71349X10 ⁻⁰¹	2.38649X10 ⁻⁰⁵	4.13043X10 ⁻⁰⁵	6.51693X10 ⁻⁰⁵
7000	5.71869X10 ⁻⁰¹	4.27747X10 ⁻⁰¹	4.91497X10 ⁻⁰⁵	1.42563X10 ⁻⁰⁴	1.91713X10 ⁻⁰⁴
7500	4.09340X10 ⁻⁰¹	5.89712X10 ⁻⁰¹	8.24086X10 ⁻⁰⁵	3.91017X10 ⁻⁰⁴	4.73425X10 ⁻⁰⁴
8000	2.68189X10 ⁻⁰¹	7.29776X10 ⁻⁰¹	1.16601X10 ⁻⁰⁴	9.00643X10 ⁻⁰⁴	1.01724X10 ⁻⁰³

$\log P/P_0 = -1.0$

T°K	X_{N_2}	X_N	$X_{N_2^+}$	X_{N^+}	X_{e^-}
2000	1.00000X10 ⁺⁰⁰	3.47030X10 ⁻¹⁰	1.44892X10 ⁻¹⁹	2.01225X10 ⁻²⁶	1.44892X10 ⁻¹⁹
2500	9.99999X10 ⁻⁰¹	1.00194X10 ⁻⁰⁷	1.44811X10 ⁻¹⁵	1.73977X10 ⁻²⁰	1.44813X10 ⁻¹⁵
3000	9.99995X10 ⁻⁰¹	4.34935X10 ⁻⁰⁶	6.93194X10 ⁻¹³	1.59914X10 ⁻¹⁶	6.93354X10 ⁻¹³
3500	9.99936X10 ⁻⁰¹	6.39854X10 ⁻⁰⁵	5.82967X10 ⁻¹¹	1.08963X10 ⁻¹³	5.84056X10 ⁻¹¹
4000	9.99521X10 ⁻⁰¹	4.79020X10 ⁻⁰⁴	1.64697X10 ⁻⁰⁹	1.45340X10 ⁻¹¹	1.66150X10 ⁻⁰⁹
4500	9.97713X10 ⁻⁰¹	2.28626X10 ⁻⁰³	2.23287X10 ⁻⁰⁸	6.49474X10 ⁻¹⁰	2.29781X10 ⁻⁰⁸
5000	9.92046X10 ⁻⁰¹	7.95353X10 ⁻⁰³	1.79142X10 ⁻⁰⁷	1.33782X10 ⁻⁰⁸	1.92521X10 ⁻⁰⁷
5500	9.78084X10 ⁻⁰¹	2.19128X10 ⁻⁰²	9.68218X10 ⁻⁰⁷	1.55200X10 ⁻⁰⁷	1.12341X10 ⁻⁰⁶
6000	9.49602X10 ⁻⁰¹	5.03875X10 ⁻⁰²	3.83543X10 ⁻⁰⁶	1.15778X10 ⁻⁰⁶	4.99322X10 ⁻⁰⁶
6500	8.99972X10 ⁻⁰¹	9.99915X10 ⁻⁰²	1.18017X10 ⁻⁰⁵	6.09298X10 ⁻⁰⁶	1.78947X10 ⁻⁰⁵
7000	8.24848X10 ⁻⁰¹	1.75044X10 ⁻⁰¹	2.94212X10 ⁻⁰⁵	2.42121X10 ⁻⁰⁵	5.36333X10 ⁻⁰⁵
7500	7.25096X10 ⁻⁰¹	2.74628X10 ⁻⁰¹	6.13583X10 ⁻⁰⁵	7.65403X10 ⁻⁰⁵	1.37898X10 ⁻⁰⁴
8000	6.07998X10 ⁻⁰¹	3.91379X10 ⁻⁰¹	1.09848X10 ⁻⁰⁴	2.00718X10 ⁻⁰⁴	3.10566X10 ⁻⁰⁴

$\log P/P_0 = 0$

Table X Mole fractions

$T^{\circ}K$	X_{N_2}	X_N	$X_{N_2^+}$	X_{N^+}	X_{e^-}
2000	1.00000X10 ⁻⁰⁰	1.09740X10 ⁻¹⁰	4.58189X10 ⁻²⁰	2.01225X10 ⁻²⁷	4.58189X10 ⁻²⁰
2500	1.00000X10 ⁻⁰⁰	3.16843X10 ⁻⁰⁸	4.57936X10 ⁻¹⁶	1.73978X10 ⁻²¹	4.57937X10 ⁻¹⁶
3000	9.99998X10 ⁻⁰¹	1.37539X10 ⁻⁰⁶	2.19224X10 ⁻¹³	1.59926X10 ⁻¹⁷	2.19240X10 ⁻¹³
3500	9.99979X10 ⁻⁰¹	2.02346X10 ⁻⁰⁵	1.84474X10 ⁻¹¹	1.09035X10 ⁻¹⁴	1.84583X10 ⁻¹¹
4000	9.99848X10 ⁻⁰¹	1.51516X10 ⁻⁰⁴	5.22512X10 ⁻¹⁰	1.45801X10 ⁻¹²	5.23970X10 ⁻¹⁰
4500	9.99276X10 ⁻⁰¹	7.23829X10 ⁻⁰⁴	7.13858X10 ⁻⁰⁹	6.56357X10 ⁻¹¹	7.20421X10 ⁻⁰⁹
5000	9.97474X10 ⁻⁰¹	2.52543X10 ⁻⁰³	5.82845X10 ⁻⁰⁸	1.37454X10 ⁻⁰⁹	5.96590X10 ⁻⁰⁸
5500	9.92991X10 ⁻⁰¹	7.00831X10 ⁻⁰³	3.25442X10 ⁻⁰⁷	1.64339X10 ⁻⁰⁸	3.41876X10 ⁻⁰⁷
6000	9.83639X10 ⁻⁰¹	1.63579X10 ⁻⁰²	1.35792X10 ⁻⁰⁶	1.28469X10 ⁻⁰⁷	1.48638X10 ⁻⁰⁶
6500	9.66648X10 ⁻⁰¹	3.33405X10 ⁻⁰²	4.49848X10 ⁻⁰⁶	7.20975X10 ⁻⁰⁷	5.21946X10 ⁻⁰⁶
7000	9.39085X10 ⁻⁰¹	6.08837X10 ⁻⁰²	1.23509X10 ⁻⁰⁵	3.10523X10 ⁻⁰⁶	1.54561X10 ⁻⁰⁵
7500	8.98502X10 ⁻⁰¹	1.01417X10 ⁻⁰¹	2.90032X10 ⁻⁰⁵	1.07822X10 ⁻⁰⁵	3.97855X10 ⁻⁰⁵
8000	8.43695X10 ⁻⁰¹	1.56122X10 ⁻⁰¹	5.96578X10 ⁻⁰⁵	3.13362X10 ⁻⁰⁵	9.09940X10 ⁻⁰⁵

$\log P/P_0 = 1.0$

Table X Mole fractions

T°K	$\frac{\partial X_{N_2}}{\partial T}$	$\frac{\partial X_N}{\partial T}$	$\frac{\partial X_{N_2}}{\partial T}$	$\frac{\partial X_{N_2}}{\partial T}$	$\frac{\partial X_{N_2}}{\partial T}$
2000	-1.55541X10 ⁻¹⁰	1.55541X10 ⁻¹⁰	1.05264X10 ⁻¹⁹	1.05265X10 ⁻¹⁹	
2500	-2.86961X10 ⁻⁰⁸	2.86961X10 ⁻⁰⁸	6.76368X10 ⁻¹⁶	6.76749X10 ⁻¹⁶	
3000	-8.63381X10 ⁻⁰⁷	8.63380X10 ⁻⁰⁷	2.24889X10 ⁻¹³	2.27311X10 ⁻¹³	
3500	-9.29036X10 ⁻⁰⁶	9.29033X10 ⁻⁰⁶	1.34565X10 ⁻¹¹	1.46302X10 ⁻¹¹	
4000	-5.21641X10 ⁻⁰⁵	5.21634X10 ⁻⁰⁵	2.53191X10 ⁻¹⁰	3.58850X10 ⁻¹⁰	
4500	-1.81048X10 ⁻⁰⁴	1.81039X10 ⁻⁰⁴	1.95856X10 ⁻⁰⁹	4.77883X10 ⁻⁰⁹	
5000	-4.00440X10 ⁻⁰⁴	4.00364X10 ⁻⁰⁴	7.37815X10 ⁻⁰⁹	3.80275X10 ⁻⁰⁸	
5500	-5.42564X10 ⁻⁰⁴	5.42194X10 ⁻⁰⁴	1.44835X10 ⁻⁰⁸	1.85080X10 ⁻⁰⁷	
6000	-4.44488X10 ⁻⁰⁴	4.43265X10 ⁻⁰⁴	1.46387X10 ⁻⁰⁸	6.11536X10 ⁻⁰⁷	
6500	-2.31539X10 ⁻⁰⁴	2.28330X10 ⁻⁰⁴	6.97024X10 ⁻⁰⁹	1.60443X10 ⁻⁰⁶	
7000	-8.84382X10 ⁻⁰⁵	8.11327X10 ⁻⁰⁵	5.59510X10 ⁻¹⁰	3.65218X10 ⁻⁰⁶	
7500	-3.06000X10 ⁻⁰⁵	1.58024X10 ⁻⁰⁵	-1.90906X10 ⁻⁰⁹	7.40071X10 ⁻⁰⁶	
8000	-1.09696X10 ⁻⁰⁵	-1.60896X10 ⁻⁰⁵	-2.62454X10 ⁻⁰⁹	1.35322X10 ⁻⁰⁵	

$\log \rho_p = -3.0$

T°K	$\frac{\partial X_{N_2}}{\partial T}$	$\frac{\partial X_N}{\partial T}$	$\frac{\partial X_{N_2}}{\partial T}$	$\frac{\partial X_{N_2}}{\partial T}$	$\frac{\partial X_{N_2}}{\partial T}$
2000	-4.91864X10 ⁻¹¹	4.91864X10 ⁻¹¹	3.32876X10 ⁻²⁰	3.32877X10 ⁻²⁰	
2500	-9.07455X10 ⁻⁰⁹	9.07455X10 ⁻⁰⁹	2.13928X10 ⁻¹⁶	2.13966X10 ⁻¹⁶	
3000	-2.73063X10 ⁻⁰⁷	2.73063X10 ⁻⁰⁷	7.13851X10 ⁻¹⁴	7.16281X10 ⁻¹⁴	
3500	-2.94397X10 ⁻⁰⁶	2.94396X10 ⁻⁰⁶	4.38492X10 ⁻¹²	4.50543X10 ⁻¹²	
4000	-1.67525X10 ⁻⁰⁵	1.67523X10 ⁻⁰⁵	9.08891X10 ⁻¹¹	1.02693X10 ⁻¹⁰	
4500	-6.15356X10 ⁻⁰⁵	6.15331X10 ⁻⁰⁵	8.60069X10 ⁻¹⁰	1.23323X10 ⁻⁰⁹	
5000	-1.60288X10 ⁻⁰⁴	1.60269X10 ⁻⁰⁴	4.39088X10 ⁻⁰⁹	9.47486X10 ⁻⁰⁹	
5500	-3.03532X10 ⁻⁰⁴	3.03432X10 ⁻⁰⁴	1.34681X10 ⁻⁰⁸	4.99463X10 ⁻⁰⁸	
6000	-4.15044X10 ⁻⁰⁴	4.14671X10 ⁻⁰⁴	2.63259X10 ⁻⁰⁸	1.86291X10 ⁻⁰⁷	
6500	-4.10638X10 ⁻⁰⁴	4.09598X10 ⁻⁰⁴	3.36224X10 ⁻⁰⁸	5.20191X10 ⁻⁰⁷	
7000	-3.01835X10 ⁻⁰⁴	2.99463X10 ⁻⁰⁴	2.81658X10 ⁻⁰⁸	1.18627X10 ⁻⁰⁶	
7500	-1.72723X10 ⁻⁰⁴	1.67957X10 ⁻⁰⁴	1.49934X10 ⁻⁰⁸	2.38337X10 ⁻⁰⁶	
8000	-8.33765X10 ⁻⁰⁵	7.46255X10 ⁻⁰⁵	3.93050X10 ⁻⁰⁹	4.37550X10 ⁻⁰⁶	

$\log \rho_p = 2.0$

Table XI Temperature derivatives of mole fractions
(density constant)

$T^{\circ}K$	$\frac{\partial X_M}{\partial T}$	$\frac{\partial X_M}{\partial T}$	$\frac{\partial X_M}{\partial T}$	$\frac{\partial X_M}{\partial T}$	$\frac{\partial X_M}{\partial T}$
2000	-1.55541X10 ⁻¹¹	1.55541X10 ⁻¹¹	1.05264X10 ⁻²⁰	6.87153X10 ⁻²⁷	1.05264X10 ⁻²⁰
2500	-2.86963X10 ⁻⁰⁹	2.86963X10 ⁻⁰⁹	6.76542X10 ⁻¹⁷	3.80836X10 ⁻²¹	6.76580X10 ⁻¹⁷
3000	-8.63541X10 ⁻⁰⁸	8.63541X10 ⁻⁰⁸	2.26010X10 ⁻¹⁴	2.43284X10 ⁻¹⁷	2.26253X10 ⁻¹⁴
3500	-9.31576X10 ⁻⁰⁷	9.31573X10 ⁻⁰⁷	1.40024X10 ⁻¹²	1.21557X10 ⁻¹⁴	1.441240X10 ⁻¹²
4000	-5.32365X10 ⁻⁰⁶	5.32359X10 ⁻⁰⁶	3.00680X10 ⁻¹¹	1.22792X10 ⁻¹²	3.12960X10 ⁻¹¹
4500	-1.99173X10 ⁻⁰⁵	1.99166X10 ⁻⁰⁵	3.11824X10 ⁻¹⁰	4.19911X10 ⁻¹¹	3.53815X10 ⁻¹⁰
5000	-5.48796X10 ⁻⁰⁵	5.48745X10 ⁻⁰⁵	1.87801X10 ⁻⁰⁹	6.55288X10 ⁻¹⁰	2.53330X10 ⁻⁰⁹
5500	-1.18386X10 ⁻⁰⁴	1.18360X10 ⁻⁰⁴	7.33889X10 ⁻⁰⁹	5.63247X10 ⁻⁰⁹	1.29713X10 ⁻⁰⁸
6000	-2.05161X10 ⁻⁰⁴	2.05060X10 ⁻⁰⁴	2.00174X10 ⁻⁰⁸	3.03953X10 ⁻⁰⁸	5.04127X10 ⁻⁰⁸
6500	-2.87915X10 ⁻⁰⁴	2.87608X10 ⁻⁰⁴	3.99793X10 ⁻⁰⁸	1.13533X10 ⁻⁰⁷	1.53513X10 ⁻⁰⁷
7000	-3.29284X10 ⁻⁰⁴	3.28528X10 ⁻⁰⁴	6.03112X10 ⁻⁰⁸	3.17618X10 ⁻⁰⁷	3.77930X10 ⁻⁰⁷
7500	-3.11257X10 ⁻⁰⁴	3.09688X10 ⁻⁰⁴	7.02139X10 ⁻⁰⁸	7.14165X10 ⁻⁰⁷	7.84379X10 ⁻⁰⁷
8000	-2.48329X10 ⁻⁰⁴	2.45452X10 ⁻⁰⁴	6.39023X10 ⁻⁰⁸	1.37449X10 ⁻⁰⁶	1.43839X10 ⁻⁰⁶

$\log \rho = -1.0$

$T^{\circ}K$	$\frac{\partial X_M}{\partial T}$	$\frac{\partial X_M}{\partial T}$	$\frac{\partial X_M}{\partial T}$	$\frac{\partial X_M}{\partial T}$	$\frac{\partial X_M}{\partial T}$
2000	-4.91864X10 ⁻¹²	4.91864X10 ⁻¹²	3.32876X10 ⁻²¹	6.87154X10 ⁻²⁸	3.32876X10 ⁻²¹
2500	-9.07457X10 ⁻¹⁰	9.07457X10 ⁻¹⁰	2.13945X10 ⁻¹⁷	3.80842X10 ⁻²²	2.13949X10 ⁻¹⁷
3000	-2.73079X10 ⁻⁰⁸	2.73079X10 ⁻⁰⁸	7.14977X10 ⁻¹⁵	2.43365X10 ⁻¹⁸	7.15221X10 ⁻¹⁵
3500	-2.94651X10 ⁻⁰⁷	2.94650X10 ⁻⁰⁷	4.44180X10 ⁻¹³	1.21892X10 ⁻¹⁵	4.45398X10 ⁻¹³
4000	-1.68610X10 ⁻⁰⁶	1.68608X10 ⁻⁰⁶	9.65079X10 ⁻¹²	1.24400X10 ⁻¹³	9.77519X10 ⁻¹²
4500	-6.34522X10 ⁻⁰⁶	6.34501X10 ⁻⁰⁶	1.03509X10 ⁻¹⁰	4.37931X10 ⁻¹²	1.07888X10 ⁻¹⁰
5000	-1.78058X10 ⁻⁰⁵	1.78043X10 ⁻⁰⁵	6.69194X10 ⁻¹⁰	7.25540X10 ⁻¹¹	7.441748X10 ⁻¹⁰
5500	-4.01603X10 ⁻⁰⁵	4.01530X10 ⁻⁰⁵	2.94433X10 ⁻⁰⁹	6.86680X10 ⁻¹⁰	3.63101X10 ⁻⁰⁹
6000	-7.60719X10 ⁻⁰⁵	7.60444X10 ⁻⁰⁵	9.52838X10 ⁻⁰⁹	4.21916X10 ⁻⁰⁹	1.37475X10 ⁻⁰⁸
6500	-1.24005X10 ⁻⁰⁴	1.23920X10 ⁻⁰⁴	2.39025X10 ⁻⁰⁸	1.84055X10 ⁻⁰⁸	4.23081X10 ⁻⁰⁸
7000	-1.76251X10 ⁻⁰⁴	1.76033X10 ⁻⁰⁴	4.82219X10 ⁻⁰⁸	6.09010X10 ⁻⁰⁸	1.09123X10 ⁻⁰⁷
7500	-2.20262X10 ⁻⁰⁴	2.19779X10 ⁻⁰⁴	8.03484X10 ⁻⁰⁸	1.60919X10 ⁻⁰⁷	2.41267X10 ⁻⁰⁷
8000	-2.44036X10 ⁻⁰⁴	2.43102X10 ⁻⁰⁴	1.12840X10 ⁻⁰⁷	3.54381X10 ⁻⁰⁷	4.67222X10 ⁻⁰⁷

$\log \rho = 0$

Table XI (Cont.) Temperature derivatives of mole fractions
(density constant)

T°K	$\frac{\partial X_{N_2}}{\partial T}$	$\frac{\partial X_{N_2}}{\partial T}$	$\frac{\partial X_{N_2}}{\partial T}$	$\frac{\partial X_{N_2}}{\partial T}$	$\frac{\partial X_{N_2}}{\partial T}$
2000	-1.55541X10 ⁻¹²	1.55541X10 ⁻¹²	1.05264X10 ⁻²¹	6.87154X10 ⁻²⁹	1.05264X10 ⁻²¹
2500	-2.86963X10 ⁻¹⁰	2.86963X10 ⁻¹⁰	6.76559X10 ⁻¹⁸	3.80844X10 ⁻²³	6.76563X10 ⁻¹⁸
3000	-8.63557X10 ⁻⁰⁹	8.63557X10 ⁻⁰⁹	2.26122X10 ⁻¹⁵	2.43391X10 ⁻¹⁹	2.26147X10 ⁻¹⁵
3500	-9.31830X10 ⁻⁰⁸	9.31828X10 ⁻⁰⁸	1.40601X10 ⁻¹³	1.21998X10 ⁻¹⁶	1.40723X10 ⁻¹³
4000	-5.33455X10 ⁻⁰⁷	5.33449X10 ⁻⁰⁷	3.06643X10 ⁻¹²	1.24920X10 ⁻¹⁴	3.07892X10 ⁻¹²
4500	-2.01125X10 ⁻⁰⁶	2.01118X10 ⁻⁰⁶	3.32597X10 ⁻¹¹	4.44040X10 ⁻¹³	3.37037X10 ⁻¹¹
5000	-5.67693X10 ⁻⁰⁶	5.67647X10 ⁻⁰⁶	2.20545X10 ⁻¹⁰	7.51685X10 ⁻¹²	2.28062X10 ⁻¹⁰
5500	-1.29905X10 ⁻⁰⁵	1.29883X10 ⁻⁰⁵	1.01679X10 ⁻⁰⁹	7.39646X10 ⁻¹¹	1.09076X10 ⁻⁰⁹
6000	-2.53543X10 ⁻⁰⁵	2.53462X10 ⁻⁰⁵	3.54354X10 ⁻⁰⁹	4.82447X10 ⁻¹⁰	4.02599X10 ⁻⁰⁹
6500	-4.36070X10 ⁻⁰⁵	4.35827X10 ⁻⁰⁵	9.87715X10 ⁻⁰⁹	2.28283X10 ⁻⁰⁹	1.21599X10 ⁻⁰⁸
7000	-6.74889X10 ⁻⁰⁵	6.74264X10 ⁻⁰⁵	2.29062X10 ⁻⁰⁸	8.35590X10 ⁻⁰⁹	3.12621X10 ⁻⁰⁸
7500	-9.52650X10 ⁻⁰⁵	9.51244X10 ⁻⁰⁵	4.54745X10 ⁻⁰⁸	2.48072X10 ⁻⁰⁸	7.02818X10 ⁻⁰⁸
8000	-1.23760X10 ⁻⁰⁴	1.23478X10 ⁻⁰⁴	7.89326X10 ⁻⁰⁸	6.19356X10 ⁻⁰⁸	1.40868X10 ⁻⁰⁷

$\log P/P_0 = 1.0$

Table XI (Cont.) Temperature derivatives of mole fractions
(density constant)

T°K	$\frac{\partial X_A}{\partial \eta}$	$\frac{\partial X_A}{\partial \eta}$	$\frac{\partial X_A}{\partial \eta}$	$\frac{\partial X_A}{\partial \eta}$
2000	5.48703X10 ⁻⁰⁶	-5.48703X10 ⁻⁰⁶	-2.29093X10 ⁻¹⁵	-2.29093X10 ⁻¹⁵
2500	1.58421X10 ⁻⁰³	-1.58421X10 ⁻⁰³	-2.28880X10 ⁻¹¹	-2.29054X10 ⁻¹¹
3000	6.87554X10 ⁻⁰²	-6.87554X10 ⁻⁰²	-1.08800X10 ⁻⁰⁸	-1.10391X10 ⁻⁰⁸
3500	1.00868X10 ⁻⁰⁰	-1.00868X10 ⁻⁰⁰	-8.68811X10 ⁻⁰⁷	-9.73152X10 ⁻⁰⁷
4000	7.40728X10 ⁻⁰⁰	-7.40722X10 ⁻⁰⁰	-2.00976X10 ⁻⁰⁵	-3.21554X10 ⁻⁰⁵
4500	3.25617X10 ⁻⁰¹	-3.25606X10 ⁻⁰¹	-1.71662X10 ⁻⁰⁴	-5.65380X10 ⁻⁰⁴
5000	8.89041X10 ⁻⁰¹	-8.88928X10 ⁻⁰¹	-6.04889X10 ⁻⁰⁴	-5.65446X10 ⁻⁰³
5500	1.45598X10 ⁻⁰²	-1.45532X10 ⁻⁰²	-5.53305X10 ⁻⁰⁴	-3.27921X10 ⁻⁰²
6000	1.41683X10 ⁻⁰²	-1.41433X10 ⁻⁰²	1.97589X10 ⁻⁰³	-1.25301X10 ⁻⁰¹
6500	8.65565X10 ⁻⁰¹	-8.57970X10 ⁻⁰¹	6.50827X10 ⁻⁰³	-3.79733X10 ⁻⁰¹
7000	3.89261X10 ⁻⁰¹	-3.69269X10 ⁻⁰¹	9.66736X10 ⁻⁰³	-9.99620X10 ⁻⁰¹
7500	1.72504X10 ⁻⁰¹	-1.26051X10 ⁻⁰¹	1.06384X10 ⁻⁰²	-2.32265X10 ⁻⁰⁰
8000	1.08882X10 ⁻⁰¹	-1.23512X10 ⁻⁰⁰	1.05336X10 ⁻⁰²	-4.82654X10 ⁻⁰⁰

$\log \eta = -3.0$

T°K	$\frac{\partial X_A}{\partial \eta}$	$\frac{\partial X_A}{\partial \eta}$	$\frac{\partial X_A}{\partial \eta}$	$\frac{\partial X_A}{\partial \eta}$
2000	1.73515X10 ⁻⁰⁷	-1.73515X10 ⁻⁰⁷	-7.24460X10 ⁻¹⁷	-7.24462X10 ⁻¹⁷
2500	5.00972X10 ⁻⁰⁵	-5.00972X10 ⁻⁰⁵	-7.23973X10 ⁻¹³	-7.24147X10 ⁻¹³
3000	2.17454X10 ⁻⁰³	-2.17454X10 ⁻⁰³	-3.45817X10 ⁻¹⁰	-3.47414X10 ⁻¹⁰
3500	3.19636X10 ⁻⁰²	-3.19635X10 ⁻⁰²	-2.86151X10 ⁻⁰⁸	-2.96903X10 ⁻⁰⁸
4000	2.37884X10 ⁻⁰¹	-2.37883X10 ⁻⁰¹	-7.55333X10 ⁻⁰⁷	-8.91960X10 ⁻⁰⁷
4500	1.10672X10 ⁻⁰⁰	-1.10669X10 ⁻⁰⁰	-8.52878X10 ⁻⁰⁶	-1.39072X10 ⁻⁰⁵
5000	3.55868X10 ⁻⁰⁰	-3.55841X10 ⁻⁰⁰	-4.79945X10 ⁻⁰⁵	-1.35990X10 ⁻⁰⁴
5500	8.14531X10 ⁻⁰⁰	-8.14355X10 ⁻⁰⁰	-1.44817X10 ⁻⁰⁴	-8.81401X10 ⁻⁰⁴
6000	1.32265X10 ⁻⁰¹	-1.32187X10 ⁻⁰¹	-2.09856X10 ⁻⁰⁴	-3.89132X10 ⁻⁰³
6500	1.53110X10 ⁻⁰¹	-1.52859X10 ⁻⁰¹	3.82705X10 ⁻⁰⁵	-1.25101X10 ⁻⁰²
7000	1.30095X10 ⁻⁰¹	-1.29445X10 ⁻⁰¹	7.82970X10 ⁻⁰⁴	-3.24976X10 ⁻⁰²
7500	8.54363X10 ⁻⁰⁰	-8.39488X10 ⁻⁰⁰	1.74832X10 ⁻⁰³	-7.43740X10 ⁻⁰²
8000	4.76786X10 ⁻⁰⁰	-4.45742X10 ⁻⁰⁰	2.46998X10 ⁻⁰³	-1.55217X10 ⁻⁰¹

$\log \eta = -2.0$

Table XII Density derivatives of mole fractions
(temperature constant)

T°K	$\frac{\partial X_{H_2}}{\partial p}$	$\frac{\partial X_{H_2}}{\partial p}$	$\frac{\partial X_{H_2}}{\partial p}$	$\frac{\partial X_{H_2}}{\partial p}$	$\frac{\partial X_{H_2}}{\partial p}$	$\frac{\partial X_{H_2}}{\partial p}$
2000	5.48703X10 ⁻⁰⁹	-5.48703X10 ⁻⁰⁹	-2.29094X10 ⁻¹⁸	-2.01225X10 ⁻²⁴	-2.29095X10 ⁻¹⁸	-2.29095X10 ⁻¹⁸
2500	1.58421X10 ⁻⁰⁶	-1.58421X10 ⁻⁰⁶	-2.28959X10 ⁻¹⁴	-1.73977X10 ⁻¹⁸	-2.28977X10 ⁻¹⁴	-2.28977X10 ⁻¹⁴
3000	6.87681X10 ⁻⁰⁵	-6.87681X10 ⁻⁰⁵	-1.09534X10 ⁻¹¹	-1.59843X10 ⁻¹⁴	-1.09694X10 ⁻¹¹	-1.09694X10 ⁻¹¹
3500	1.01144X10 ⁻⁰³	-1.01144X10 ⁻⁰³	-9.16961X10 ⁻¹⁰	-1.08571X10 ⁻¹¹	-9.27818X10 ⁻¹⁰	-9.27818X10 ⁻¹⁰
4000	7.55957X10 ⁻⁰³	-7.55957X10 ⁻⁰³	-2.53985X10 ⁻⁰⁸	-1.42878X10 ⁻⁰⁹	-2.68273X10 ⁻⁰⁸	-2.68273X10 ⁻⁰⁸
4500	3.58215X10 ⁻⁰²	-3.58215X10 ⁻⁰²	-3.25177X10 ⁻⁰⁷	-6.14495X10 ⁻⁰⁸	-3.86626X10 ⁻⁰⁷	-3.86626X10 ⁻⁰⁷
5000	1.21842X10 ⁻⁰¹	-1.21842X10 ⁻⁰¹	-2.30622X10 ⁻⁰⁶	-1.16905X10 ⁻⁰⁶	-3.47527X10 ⁻⁰⁶	-3.47527X10 ⁻⁰⁶
5500	3.17693X10 ⁻⁰¹	-3.17693X10 ⁻⁰¹	-1.00576X10 ⁻⁰⁵	-1.19178X10 ⁻⁰⁵	-2.19754X10 ⁻⁰⁵	-2.19754X10 ⁻⁰⁵
6000	6.53807X10 ⁻⁰¹	-6.53807X10 ⁻⁰¹	-2.86084X10 ⁻⁰⁵	-7.45237X10 ⁻⁰⁵	-1.03132X10 ⁻⁰⁴	-1.03132X10 ⁻⁰⁴
6500	1.07338X10 ⁺⁰⁰	-1.07264X10 ⁺⁰⁰	-5.33043X10 ⁻⁰⁵	-3.16366X10 ⁻⁰⁴	-3.69670X10 ⁻⁰⁴	-3.69670X10 ⁻⁰⁴
7000	1.41791X10 ⁺⁰⁰	-1.41582X10 ⁺⁰⁰	-5.69228X10 ⁻⁰⁵	-9.90168X10 ⁻⁰⁴	-1.04709X10 ⁻⁰³	-1.04709X10 ⁻⁰³
7500	1.53139X10 ⁺⁰⁰	-1.52647X10 ⁺⁰⁰	1.86361X10 ⁻⁰⁶	-2.46349X10 ⁻⁰³	-2.46163X10 ⁻⁰³	-2.46163X10 ⁻⁰³
8000	1.38389X10 ⁺⁰⁰	-1.37374X10 ⁺⁰⁰	1.42940X10 ⁻⁰⁴	-5.21973X10 ⁻⁰³	-5.07679X10 ⁻⁰³	-5.07679X10 ⁻⁰³
$\log p/p_0 = -1.0$						
T°K	$\frac{\partial X_{H_2}}{\partial p}$	$\frac{\partial X_{H_2}}{\partial p}$	$\frac{\partial X_{H_2}}{\partial p}$	$\frac{\partial X_{H_2}}{\partial p}$	$\frac{\partial X_{H_2}}{\partial p}$	$\frac{\partial X_{H_2}}{\partial p}$
2000	1.73515X10 ⁻¹⁰	-1.73515X10 ⁻¹⁰	-7.24461X10 ⁻²⁰	-2.01225X10 ⁻²⁶	-7.24461X10 ⁻²⁰	-7.24461X10 ⁻²⁰
2500	5.00973X10 ⁻⁰⁸	-5.00973X10 ⁻⁰⁸	-7.24053X10 ⁻¹⁶	-1.73977X10 ⁻²⁰	-7.24070X10 ⁻¹⁶	-7.24070X10 ⁻¹⁶
3000	2.17467X10 ⁻⁰⁶	-2.17467X10 ⁻⁰⁶	-3.46555X10 ⁻¹³	-1.59904X10 ⁻¹⁶	-3.46715X10 ⁻¹³	-3.46715X10 ⁻¹³
3500	3.19912X10 ⁻⁰⁵	-3.19911X10 ⁻⁰⁵	-2.91197X10 ⁻¹¹	-1.08911X10 ⁻¹³	-2.92286X10 ⁻¹¹	-2.92286X10 ⁻¹¹
4000	2.39426X10 ⁻⁰⁴	-2.39424X10 ⁻⁰⁴	-8.19589X10 ⁻¹⁰	-1.45005X10 ⁻¹¹	-8.34089X10 ⁻¹⁰	-8.34089X10 ⁻¹⁰
4500	1.14119X10 ⁻⁰³	-1.14117X10 ⁻⁰³	-1.09873X10 ⁻⁰⁸	-6.44511X10 ⁻¹⁰	-1.16318X10 ⁻⁰⁸	-1.16318X10 ⁻⁰⁸
5000	3.95322X10 ⁻⁰³	-3.95303X10 ⁻⁰³	-8.59184X10 ⁻⁰⁸	-1.31188X10 ⁻⁰⁸	-9.90372X10 ⁻⁰⁸	-9.90372X10 ⁻⁰⁸
5500	1.07771X10 ⁻⁰²	-1.07760X10 ⁻⁰²	-4.42511X10 ⁻⁰⁷	-1.48965X10 ⁻⁰⁷	-5.91476X10 ⁻⁰⁷	-5.91476X10 ⁻⁰⁷
6000	2.42427X10 ⁻⁰²	-2.42373X10 ⁻⁰²	-1.61968X10 ⁻⁰⁶	-1.07539X10 ⁻⁰⁶	-2.69507X10 ⁻⁰⁶	-2.69507X10 ⁻⁰⁶
6500	4.62313X10 ⁻⁰²	-4.62116X10 ⁻⁰²	-4.42251X10 ⁻⁰⁶	-5.41204X10 ⁻⁰⁶	-9.83456X10 ⁻⁰⁶	-9.83456X10 ⁻⁰⁶
7000	7.58921X10 ⁻⁰²	-7.58329X10 ⁻⁰²	-9.25823X10 ⁻⁰⁶	-2.03347X10 ⁻⁰⁵	-2.95929X10 ⁻⁰⁵	-2.95929X10 ⁻⁰⁵
7500	1.08338X10 ⁻⁰¹	-1.08187X10 ⁻⁰¹	-1.49215X10 ⁻⁰⁵	-6.01917X10 ⁻⁰⁵	-7.51133X10 ⁻⁰⁵	-7.51133X10 ⁻⁰⁵
8000	1.35822X10 ⁻⁰¹	-1.35492X10 ⁻⁰¹	-1.78221X10 ⁻⁰⁵	-1.46822X10 ⁻⁰⁴	-1.64644X10 ⁻⁰⁴	-1.64644X10 ⁻⁰⁴
$\log p/p_0 = 0$						

Table XII (Cont.) Density derivatives of mole fractions
(temperature constant)

T°K	$\frac{\partial x_{N_2}}{\partial \rho}$	$\frac{\partial x_{N_2}}{\partial \rho}$	$\frac{\partial x_{N_2}}{\partial \rho}$	$\frac{\partial x_{N_2}}{\partial \rho}$	$\frac{\partial x_{N_2}}{\partial \rho}$	$\frac{\partial x_{N_2}}{\partial \rho}$
2000	5.48703X10 ⁻¹²	-5.48703X10 ⁻¹²	-2.29094X10 ⁻²¹	-2.29094X10 ⁻²¹	-2.29094X10 ⁻²¹	-2.29094X10 ⁻²¹
2500	1.58421X10 ⁻⁰⁹	-1.58421X10 ⁻⁰⁹	-2.28967X10 ⁻¹⁷	-2.28967X10 ⁻¹⁷	-2.28967X10 ⁻¹⁷	-2.28967X10 ⁻¹⁷
3000	6.87694X10 ⁻⁰⁸	-6.87694X10 ⁻⁰⁸	-1.09608X10 ⁻¹⁴	-1.09608X10 ⁻¹⁴	-1.09624X10 ⁻¹⁴	-1.09624X10 ⁻¹⁴
3500	1.01171X10 ⁻⁰⁶	-1.01171X10 ⁻⁰⁶	-9.22084X10 ⁻¹³	-9.22084X10 ⁻¹³	-9.23174X10 ⁻¹³	-9.23174X10 ⁻¹³
4000	7.57504X10 ⁻⁰⁶	-7.57499X10 ⁻⁰⁶	-2.60862X10 ⁻¹¹	-2.60862X10 ⁻¹¹	-2.62319X10 ⁻¹¹	-2.62319X10 ⁻¹¹
4500	3.61725X10 ⁻⁰⁵	-3.61718X10 ⁻⁰⁵	-3.55109X10 ⁻¹⁰	-3.55109X10 ⁻¹⁰	-3.61656X10 ⁻¹⁰	-3.61656X10 ⁻¹⁰
5000	1.26038X10 ⁻⁰⁴	-1.26032X10 ⁻⁰⁴	-2.87511X10 ⁻⁰⁹	-2.87511X10 ⁻⁰⁹	-3.01168X10 ⁻⁰⁹	-3.01168X10 ⁻⁰⁹
5500	3.48607X10 ⁻⁰⁴	-3.48572X10 ⁻⁰⁴	-1.57947X10 ⁻⁰⁸	-1.57947X10 ⁻⁰⁸	-1.74155X10 ⁻⁰⁸	-1.74155X10 ⁻⁰⁸
6000	8.08001X10 ⁻⁰⁴	-8.07847X10 ⁻⁰⁴	-6.41155X10 ⁻⁰⁸	-6.41155X10 ⁻⁰⁸	-7.66313X10 ⁻⁰⁸	-7.66313X10 ⁻⁰⁸
6500	1.62576X10 ⁻⁰³	-1.62521X10 ⁻⁰³	-2.03615X10 ⁻⁰⁷	-2.03615X10 ⁻⁰⁷	-2.72606X10 ⁻⁰⁷	-2.72606X10 ⁻⁰⁷
7000	2.90603X10 ⁻⁰³	-2.90440X10 ⁻⁰³	-5.26166X10 ⁻⁰⁷	-5.26166X10 ⁻⁰⁷	-8.16190X10 ⁻⁰⁷	-8.16190X10 ⁻⁰⁷
7500	4.68568X10 ⁻⁰³	-4.68145X10 ⁻⁰³	-1.13690X10 ⁻⁰⁶	-1.13690X10 ⁻⁰⁶	-2.11345X10 ⁻⁰⁶	-2.11345X10 ⁻⁰⁶
8000	6.88748X10 ⁻⁰³	-6.87783X10 ⁻⁰³	-2.09186X10 ⁻⁰⁶	-2.09186X10 ⁻⁰⁶	-4.82667X10 ⁻⁰⁶	-4.82667X10 ⁻⁰⁶

$\log P/P_0 = 1.0$

Table XII (Cont.) Density derivatives of mole fractions
(temperature constant)

T°K	$\frac{S}{R}$	$S \frac{\text{cal}}{\text{gm} \cdot ^\circ\text{K}}$	$\frac{H}{RT}$	$H \frac{\text{cal}}{\text{gm}}$	Z
2000	3.52611X10 ⁺⁰¹	2.50017X10 ⁺⁰⁰	3.89271X10 ⁺⁰⁰	5.52060X10 ⁺⁰²	1.00000X10 ⁺⁰⁰
2500	3.60099X10 ⁺⁰¹	2.55326X10 ⁺⁰⁰	3.98563X10 ⁺⁰⁰	7.06548X10 ⁺⁰²	1.00000X10 ⁺⁰⁰
3000	3.66352X10 ⁺⁰¹	2.59760X10 ⁺⁰⁰	4.05989X10 ⁺⁰⁰	8.63654X10 ⁺⁰²	1.00006X10 ⁺⁰⁰
3500	3.71994X10 ⁺⁰¹	2.63760X10 ⁺⁰⁰	4.14745X10 ⁺⁰⁰	1.02932X10 ⁺⁰³	1.00101X10 ⁺⁰⁰
4000	3.78572X10 ⁺⁰¹	2.68425X10 ⁺⁰⁰	4.37980X10 ⁺⁰⁰	1.24227X10 ⁺⁰³	1.00754X10 ⁺⁰⁰
4500	3.90035X10 ⁺⁰¹	2.76552X10 ⁺⁰⁰	5.12284X10 ⁺⁰⁰	1.63466X10 ⁺⁰³	1.03556X10 ⁺⁰⁰
5000	4.13333X10 ⁺⁰¹	2.93071X10 ⁺⁰⁰	7.02309X10 ⁺⁰⁰	2.49001X10 ⁺⁰³	1.11877X10 ⁺⁰⁰
5500	4.54592X10 ⁺⁰¹	3.22326X10 ⁺⁰⁰	1.06143X10 ⁺⁰¹	4.13961X10 ⁺⁰³	1.29574X10 ⁺⁰⁰
6000	5.08525X10 ⁺⁰¹	3.60567X10 ⁺⁰⁰	1.52652X10 ⁺⁰¹	6.49469X10 ⁺⁰³	1.55385X10 ⁺⁰⁰
6500	5.54615X10 ⁺⁰¹	3.93247X10 ⁺⁰⁰	1.88640X10 ⁺⁰¹	8.69465X10 ⁺⁰³	1.78931X10 ⁺⁰⁰
7000	5.80444X10 ⁺⁰¹	4.11560X10 ⁺⁰⁰	2.02550X10 ⁺⁰¹	1.00539X10 ⁺⁰⁴	1.92146X10 ⁺⁰⁰
7500	5.93143X10 ⁺⁰¹	4.20565X10 ⁺⁰⁰	2.03125X10 ⁺⁰¹	1.08026X10 ⁺⁰⁴	1.97839X10 ⁺⁰⁰
8000	6.01469X10 ⁺⁰¹	4.26468X10 ⁺⁰⁰	2.00011X10 ⁺⁰¹	1.13461X10 ⁺⁰⁴	2.00745X10 ⁺⁰⁰

T°K	$\frac{S}{R}$	$S \frac{\text{cal}}{\text{gm} \cdot ^\circ\text{K}}$	$\frac{H}{RT}$	$H \frac{\text{cal}}{\text{gm}}$	Z
2000	3.29585X10 ⁺⁰¹	2.33690X10 ⁺⁰⁰	3.89271X10 ⁺⁰⁰	5.52060X10 ⁺⁰²	1.00000X10 ⁺⁰⁰
2500	3.37073X10 ⁺⁰¹	2.39000X10 ⁺⁰⁰	3.98558X10 ⁺⁰⁰	7.06539X10 ⁺⁰²	1.00000X10 ⁺⁰⁰
3000	3.43307X10 ⁺⁰¹	2.43420X10 ⁺⁰⁰	4.05807X10 ⁺⁰⁰	8.63268X10 ⁺⁰²	1.00002X10 ⁺⁰⁰
3500	3.48731X10 ⁺⁰¹	2.47266X10 ⁺⁰⁰	4.12447X10 ⁺⁰⁰	1.02362X10 ⁺⁰³	1.00031X10 ⁺⁰⁰
4000	3.53991X10 ⁺⁰¹	2.50995X10 ⁺⁰⁰	4.22943X10 ⁺⁰⁰	1.19962X10 ⁺⁰³	1.00239X10 ⁺⁰⁰
4500	3.60469X10 ⁺⁰¹	2.55589X10 ⁺⁰⁰	4.49374X10 ⁺⁰⁰	1.43392X10 ⁺⁰³	1.01138X10 ⁺⁰⁰
5000	3.70723X10 ⁺⁰¹	2.62859X10 ⁺⁰⁰	5.15178X10 ⁺⁰⁰	1.82655X10 ⁺⁰³	1.03921X10 ⁺⁰⁰
5500	3.88237X10 ⁺⁰¹	2.75277X10 ⁺⁰⁰	6.52213X10 ⁺⁰⁰	2.54364X10 ⁺⁰³	1.10538X10 ⁺⁰⁰
6000	4.15767X10 ⁺⁰¹	2.94797X10 ⁺⁰⁰	8.83990X10 ⁺⁰⁰	3.76099X10 ⁺⁰³	1.22991X10 ⁺⁰⁰
6500	4.52182X10 ⁺⁰¹	3.20617X10 ⁺⁰⁰	1.19429X10 ⁺⁰¹	5.50465X10 ⁺⁰³	1.41436X10 ⁺⁰⁰
7000	4.90274X10 ⁺⁰¹	3.47626X10 ⁺⁰⁰	1.50684X10 ⁺⁰¹	7.47945X10 ⁺⁰³	1.62232X10 ⁺⁰⁰
7500	5.20699X10 ⁺⁰¹	3.69199X10 ⁺⁰⁰	1.72783X10 ⁺⁰¹	9.18897X10 ⁺⁰³	1.79505X10 ⁺⁰⁰
8000	5.40146X10 ⁺⁰¹	3.82988X10 ⁺⁰⁰	1.82971X10 ⁺⁰¹	1.03795X10 ⁺⁰⁴	1.90371X10 ⁺⁰⁰

Table XIII Entropy, enthalpy, compressibility factor

T°K	$\frac{S}{R}$	$S \frac{\text{cal}}{\text{gm}^\circ\text{K}}$	$\frac{H}{RT}$	$H \frac{\text{cal}}{\text{gm}}$	Z
2000	3.06559X10 ⁺⁰¹	2.17364X10 ⁺⁰⁰	3.89271X10 ⁺⁰⁰	5.52060X10 ⁺⁰²	1.00000X10 ⁺⁰⁰
2500	3.14047X10 ⁺⁰¹	2.22673X10 ⁺⁰⁰	3.98557X10 ⁺⁰⁰	7.06536X10 ⁺⁰²	1.00000X10 ⁺⁰⁰
3000	3.20276X10 ⁺⁰¹	2.27090X10 ⁺⁰⁰	4.05750X10 ⁺⁰⁰	8.63145X10 ⁺⁰²	1.00000X10 ⁺⁰⁰
3500	3.25631X10 ⁺⁰¹	2.30886X10 ⁺⁰⁰	4.11720X10 ⁺⁰⁰	1.02182X10 ⁺⁰³	1.00010X10 ⁺⁰⁰
4000	3.30471X10 ⁺⁰¹	2.34319X10 ⁺⁰⁰	4.18172X10 ⁺⁰⁰	1.18609X10 ⁺⁰³	1.00075X10 ⁺⁰⁰
4500	3.35342X10 ⁺⁰¹	2.37772X10 ⁺⁰⁰	4.29153X10 ⁺⁰⁰	1.36939X10 ⁺⁰³	1.00361X10 ⁺⁰⁰
5000	3.41154X10 ⁺⁰¹	2.41894X10 ⁺⁰⁰	4.52507X10 ⁺⁰⁰	1.60435X10 ⁺⁰³	1.01257X10 ⁺⁰⁰
5500	3.49231X10 ⁺⁰¹	2.47620X10 ⁺⁰⁰	5.00087X10 ⁺⁰⁰	1.95035X10 ⁺⁰³	1.03461X10 ⁺⁰⁰
6000	3.61112X10 ⁺⁰¹	2.56045X10 ⁺⁰⁰	5.85661X10 ⁺⁰⁰	2.49173X10 ⁺⁰³	1.07947X10 ⁺⁰⁰
6500	3.78053X10 ⁺⁰¹	2.68057X10 ⁺⁰⁰	7.19858X10 ⁺⁰⁰	3.31790X10 ⁺⁰³	1.15708X10 ⁺⁰⁰
7000	4.00261X10 ⁺⁰¹	2.83803X10 ⁺⁰⁰	9.02586X10 ⁺⁰⁰	4.48013X10 ⁺⁰³	1.27248X10 ⁺⁰⁰
7500	4.26179X10 ⁺⁰¹	3.02180X10 ⁺⁰⁰	1.11615X10 ⁺⁰¹	5.93593X10 ⁺⁰³	1.41949X10 ⁺⁰⁰
8000	4.52508X10 ⁺⁰¹	3.20848X10 ⁺⁰⁰	1.32598X10 ⁺⁰¹	7.52198X10 ⁺⁰³	1.57817X10 ⁺⁰⁰

log %

T°K	$\frac{S}{R}$	$S \frac{\text{cal}}{\text{gm}^\circ\text{K}}$	$\frac{H}{RT}$	$H \frac{\text{cal}}{\text{gm}}$	Z
2000	2.83533X10 ⁺⁰¹	2.01038X10 ⁺⁰⁰	3.89271X10 ⁺⁰⁰	5.52060X10 ⁺⁰²	1.00000X10 ⁺⁰⁰
2500	2.91021X10 ⁺⁰¹	2.06347X10 ⁺⁰⁰	3.98555X10 ⁺⁰⁰	7.06535X10 ⁺⁰²	1.00000X10 ⁺⁰⁰
3000	2.97248X10 ⁺⁰¹	2.10762X10 ⁺⁰⁰	4.05731X10 ⁺⁰⁰	8.63106X10 ⁺⁰²	1.00000X10 ⁺⁰⁰
3500	3.02581X10 ⁺⁰¹	2.14543X10 ⁺⁰⁰	4.11490X10 ⁺⁰⁰	1.02125X10 ⁺⁰³	1.00003X10 ⁺⁰⁰
4000	3.07289X10 ⁺⁰¹	2.17882X10 ⁺⁰⁰	4.16662X10 ⁺⁰⁰	1.18181X10 ⁺⁰³	1.00023X10 ⁺⁰⁰
4500	3.11649X10 ⁺⁰¹	2.20973X10 ⁺⁰⁰	4.22725X10 ⁺⁰⁰	1.34888X10 ⁺⁰³	1.00114X10 ⁺⁰⁰
5000	3.16023X10 ⁺⁰¹	2.24075X10 ⁺⁰⁰	4.32328X10 ⁺⁰⁰	1.53280X10 ⁺⁰³	1.00399X10 ⁺⁰⁰
5500	3.20903X10 ⁺⁰¹	2.27534X10 ⁺⁰⁰	4.49492X10 ⁺⁰⁰	1.75302X10 ⁺⁰³	1.01107X10 ⁺⁰⁰
6000	3.26884X10 ⁺⁰¹	2.31775X10 ⁺⁰⁰	4.79339X10 ⁺⁰⁰	2.03938X10 ⁺⁰³	1.02585X10 ⁺⁰⁰
6500	3.34597X10 ⁺⁰¹	2.37244X10 ⁺⁰⁰	5.27312X10 ⁺⁰⁰	2.43044X10 ⁺⁰³	1.05265X10 ⁺⁰⁰
7000	3.44586X10 ⁺⁰¹	2.44327X10 ⁺⁰⁰	5.97942X10 ⁺⁰⁰	2.96798X10 ⁺⁰³	1.09599X10 ⁺⁰⁰
7500	3.57153X10 ⁺⁰¹	2.53237X10 ⁺⁰⁰	6.93294X10 ⁺⁰⁰	3.68708X10 ⁺⁰³	1.15940X10 ⁺⁰⁰
8000	3.72194X10 ⁺⁰¹	2.63902X10 ⁺⁰⁰	8.11430X10 ⁺⁰⁰	4.60304X10 ⁺⁰³	1.24393X10 ⁺⁰⁰

log %

Table XIII (Cont.) Entropy, enthalpy, compressibility factor

T°K	$\frac{S}{R}$	$S \frac{\text{cal}}{\text{gm}^\circ\text{K}}$	$\frac{H}{RT}$	$H \frac{\text{cal}}{\text{gm}}$	Z
2000	2.60507X10 ⁺⁰¹	1.84711X10 ⁺⁰⁰	3.89271X10 ⁺⁰⁰	5.52060X10 ⁺⁰²	1.00000X10 ⁺⁰⁰
2500	2.67995X10 ⁺⁰¹	1.90020X10 ⁺⁰⁰	3.98556X10 ⁺⁰⁰	7.06535X10 ⁺⁰²	1.00000X10 ⁺⁰⁰
3000	2.74221X10 ⁺⁰¹	1.94435X10 ⁺⁰⁰	4.05726X10 ⁺⁰⁰	8.63094X10 ⁺⁰²	1.00000X10 ⁺⁰⁰
3500	2.79548X10 ⁺⁰¹	1.98212X10 ⁺⁰⁰	4.11418X10 ⁺⁰⁰	1.02107X10 ⁺⁰³	1.00001X10 ⁺⁰⁰
4000	2.84214X10 ⁺⁰¹	2.01520X10 ⁺⁰⁰	4.16184X10 ⁺⁰⁰	1.18045X10 ⁺⁰³	1.00007X10 ⁺⁰⁰
4500	2.88411X10 ⁺⁰¹	2.04496X10 ⁺⁰⁰	4.20689X10 ⁺⁰⁰	1.34238X10 ⁺⁰³	1.00036X10 ⁺⁰⁰
5000	2.92328X10 ⁺⁰¹	2.07274X10 ⁺⁰⁰	4.25910X10 ⁺⁰⁰	1.51005X10 ⁺⁰³	1.00126X10 ⁺⁰⁰
5500	2.96175X10 ⁺⁰¹	2.10001X10 ⁺⁰⁰	4.33237X10 ⁺⁰⁰	1.68963X10 ⁺⁰³	1.00351X10 ⁺⁰⁰
6000	3.00187X10 ⁺⁰¹	2.12846X10 ⁺⁰⁰	4.44436X10 ⁺⁰⁰	1.89088X10 ⁺⁰³	1.00824X10 ⁺⁰⁰
6500	3.04618X10 ⁺⁰¹	2.15988X10 ⁺⁰⁰	4.61514X10 ⁺⁰⁰	2.12717X10 ⁺⁰³	1.01695X10 ⁺⁰⁰

Table XIII (Cont.) Entropy, enthalpy, compressibility factor

T°K	$\frac{P}{P_0}$	$\frac{\partial P}{\partial P_0}$	M _{gm.}	$\frac{\partial M}{\partial T} \frac{\text{gms}}{^\circ\text{K}}$	$\frac{\partial M}{\partial P_0}$
2000	6.94058X10 ⁻⁰³	6.94058X10 ⁺⁰⁰	2.80140X10 ⁺⁰¹	-2.17866X10 ⁻⁰⁹	7.68568X10 ⁻⁰⁵
2500	8.67573X10 ⁻⁰³	8.67573X10 ⁺⁰⁰	2.80139X10 ⁺⁰¹	-4.01947X10 ⁻⁰⁷	2.21900X10 ⁻⁰²
3000	1.04115X10 ⁻⁰²	1.04112X10 ⁺⁰¹	2.80120X10 ⁺⁰¹	-1.20933X10 ⁻⁰⁵	9.63057X10 ⁻⁰¹
3500	1.21582X10 ⁻⁰²	1.21521X10 ⁺⁰¹	2.79856X10 ⁺⁰¹	-1.30130X10 ⁻⁰⁴	1.41286X10 ⁺⁰¹
4000	1.39859X10 ⁻⁰²	1.39337X10 ⁺⁰¹	2.78041X10 ⁺⁰¹	-7.30664X10 ⁻⁰⁴	1.03754X10 ⁺⁰²
4500	1.61716X10 ⁻⁰²	1.58990X10 ⁺⁰¹	2.70519X10 ⁺⁰¹	-2.53599X10 ⁻⁰³	4.56097X10 ⁺⁰²
5000	1.94123X10 ⁻⁰²	1.84469X10 ⁺⁰¹	2.50398X10 ⁺⁰¹	-5.60939X10 ⁻⁰³	1.24535X10 ⁺⁰³
5500	2.47313X10 ⁻⁰²	2.23979X10 ⁺⁰¹	2.16200X10 ⁺⁰¹	-7.60209X10 ⁻⁰³	2.03984X10 ⁺⁰³
6000	3.23540X10 ⁻⁰²	2.87893X10 ⁺⁰¹	1.80286X10 ⁺⁰¹	-6.23431X10 ⁻⁰³	1.98634X10 ⁺⁰³
6500	4.03614X10 ⁻⁰²	3.72219X10 ⁺⁰¹	1.56562X10 ⁺⁰¹	-3.26554X10 ⁻⁰³	1.21780X10 ⁺⁰³
7000	4.66761X10 ⁻⁰²	4.48853X10 ⁺⁰¹	1.45795X10 ⁺⁰¹	-1.28991X10 ⁻⁰³	5.59375X10 ⁺⁰²
7500	5.14920X10 ⁻⁰²	5.04944X10 ⁺⁰¹	1.41599X10 ⁺⁰¹	-5.32276X10 ⁻⁰⁴	2.74309X10 ⁺⁰²
8000	5.57316X10 ⁻⁰²	5.48520X10 ⁺⁰¹	1.39549X10 ⁺⁰¹	-3.43197X10 ⁻⁰⁴	2.20264X10 ⁺⁰²
log P/P ₀ = -3.0					
T°K	$\frac{P}{P_0}$	$\frac{\partial P}{\partial P_0}$	M _{gm.}	$\frac{\partial M}{\partial T} \frac{\text{gms}}{^\circ\text{K}}$	$\frac{\partial M}{\partial P_0}$
2000	6.94058X10 ⁻⁰²	6.94058X10 ⁺⁰⁰	2.80140X10 ⁺⁰¹	-6.88954X10 ⁻¹⁰	2.43042X10 ⁻⁰⁶
2500	8.67572X10 ⁻⁰²	8.67572X10 ⁺⁰⁰	2.80139X10 ⁺⁰¹	-1.27107X10 ⁻⁰⁷	7.01712X10 ⁻⁰⁴
3000	1.04110X10 ⁻⁰¹	1.04109X10 ⁺⁰¹	2.80133X10 ⁺⁰¹	-3.82480X10 ⁻⁰⁶	3.04588X10 ⁻⁰²
3500	1.21499X10 ⁻⁰¹	1.21479X10 ⁺⁰¹	2.80050X10 ⁺⁰¹	-4.12361X10 ⁻⁰⁵	4.47714X10 ⁻⁰¹
4000	1.39143X10 ⁻⁰¹	1.38977X10 ⁺⁰¹	2.79471X10 ⁺⁰¹	-2.34652X10 ⁻⁰⁴	3.33205X10 ⁺⁰⁰
4500	1.57941X10 ⁻⁰¹	1.57057X10 ⁺⁰¹	2.76986X10 ⁺⁰¹	-8.61935X10 ⁻⁰⁴	1.55019X10 ⁺⁰¹
5000	1.80319X10 ⁻⁰¹	1.76984X10 ⁺⁰¹	2.69568X10 ⁺⁰¹	-2.24523X10 ⁻⁰³	4.98477X10 ⁺⁰¹
5500	2.10980X10 ⁻⁰¹	2.01481X10 ⁺⁰¹	2.53431X10 ⁺⁰¹	-4.25209X10 ⁻⁰³	1.14101X10 ⁺⁰²
6000	2.56090X10 ⁻⁰¹	2.35254X10 ⁺⁰¹	2.27771X10 ⁺⁰¹	-5.81576X10 ⁻⁰³	1.85315X10 ⁺⁰²
6500	3.19035X10 ⁻⁰¹	2.84463X10 ⁺⁰¹	1.98068X10 ⁺⁰¹	-5.75863X10 ⁻⁰³	2.14637X10 ⁺⁰²
7000	3.94095X10 ⁻⁰¹	3.52401X10 ⁺⁰¹	1.72678X10 ⁺⁰¹	-4.24403X10 ⁻⁰³	1.82690X10 ⁺⁰²
7500	4.67201X10 ⁻⁰¹	4.31056X10 ⁺⁰¹	1.56062X10 ⁺⁰¹	-2.45251X10 ⁻⁰³	1.20736X10 ⁺⁰²
8000	5.28515X10 ⁻⁰¹	5.03736X10 ⁺⁰¹	1.47154X10 ⁺⁰¹	-1.22908X10 ⁻⁰³	6.89922X10 ⁺⁰¹
log P/P ₀ = -2.0					

Table XIV Pressure, density derivative of pressure (temperature constant), molecular weight, temperature and density derivative of molecular weight

$T^{\circ}K$	$\frac{P}{P_0}$	$\frac{\partial P}{\partial \rho}$	M_{gm}	$\frac{\partial M}{\partial T} \frac{gms}{^{\circ}K}$	$\frac{\partial M}{\partial \rho}$
2000	6.94058X10 ⁻⁰¹	6.94058X10 ⁺⁰⁰	2.80140X10 ⁺⁰¹	-2.17866X10 ⁻¹⁰	7.68569X10 ⁻⁰⁸
2500	8.67572X10 ⁻⁰¹	8.67572X10 ⁺⁰⁰	2.80139X10 ⁺⁰¹	-4.01949X10 ⁻⁰⁸	2.21901X10 ⁻⁰⁵
3000	1.04109X10 ⁺⁰⁰	1.04109X10 ⁺⁰¹	2.80138X10 ⁺⁰¹	-1.20956X10 ⁻⁰⁶	9.63235X10 ⁻⁰⁴
3500	1.21472X10 ⁺⁰⁰	1.21466X10 ⁺⁰¹	2.80111X10 ⁺⁰¹	-1.30485X10 ⁻⁰⁵	1.41672X10 ⁻⁰²
4000	1.38916X10 ⁺⁰⁰	1.38864X10 ⁺⁰¹	2.79927X10 ⁺⁰¹	-7.45684X10 ⁻⁰⁵	1.05886X10 ⁻⁰¹
4500	1.56727X10 ⁺⁰⁰	1.56445X10 ⁺⁰¹	2.79131X10 ⁺⁰¹	-2.78982X10 ⁻⁰⁴	5.01753X10 ⁻⁰¹
5000	1.75695X10 ⁺⁰⁰	1.74612X10 ⁺⁰¹	2.76661X10 ⁺⁰¹	-7.68707X10 ⁻⁰⁴	1.70666X10 ⁺⁰⁰
5500	1.97473X10 ⁺⁰⁰	1.94227X10 ⁺⁰¹	2.70766X10 ⁺⁰¹	-1.65831X10 ⁻⁰³	4.45010X10 ⁺⁰⁰
6000	2.24764X10 ⁺⁰⁰	2.16832X10 ⁺⁰¹	2.59515X10 ⁺⁰¹	-2.87412X10 ⁻⁰³	9.15892X10 ⁺⁰⁰
6500	2.61002X10 ⁺⁰⁰	2.44789X10 ⁺⁰¹	2.42108X10 ⁺⁰¹	-4.03442X10 ⁻⁰³	1.50393X10 ⁺⁰¹
7000	3.09112X10 ⁺⁰⁰	2.81206X10 ⁺⁰¹	2.20151X10 ⁺⁰¹	-4.61673X10 ⁻⁰³	1.98746X10 ⁺⁰¹
7500	3.69455X10 ⁺⁰⁰	3.29234X10 ⁺⁰¹	1.97351X10 ⁺⁰¹	-4.36978X10 ⁻⁰³	2.14847X10 ⁺⁰¹
8000	4.38137X10 ⁺⁰⁰	3.90111X10 ⁺⁰¹	1.77509X10 ⁺⁰¹	-3.49760X10 ⁻⁰³	1.94573X10 ⁺⁰¹
$\log P/P_0 = -1.0$					
$T^{\circ}K$	$\frac{P}{P_0}$	$\frac{\partial P}{\partial \rho}$	M_{gm}	$\frac{\partial M}{\partial T} \frac{gms}{^{\circ}K}$	$\frac{\partial M}{\partial \rho}$
2000	6.94058X10 ⁺⁰⁰	6.94058X10 ⁺⁰⁰	2.80140X10 ⁺⁰¹	-6.88954X10 ⁻¹¹	2.43042X10 ⁻⁰⁹
2500	8.67572X10 ⁺⁰⁰	8.67572X10 ⁺⁰⁰	2.80140X10 ⁺⁰¹	-1.27107X10 ⁻⁰⁸	7.01713X10 ⁻⁰⁷
3000	1.04108X10 ⁺⁰¹	1.04108X10 ⁺⁰¹	2.80139X10 ⁺⁰¹	-3.82502X10 ⁻⁰⁷	3.04606X10 ⁻⁰⁵
3500	1.21464X10 ⁺⁰¹	1.21462X10 ⁺⁰¹	2.80131X10 ⁺⁰¹	-4.12718X10 ⁻⁰⁶	4.48101X10 ⁻⁰⁴
4000	1.38844X10 ⁺⁰¹	1.38828X10 ⁺⁰¹	2.80072X10 ⁺⁰¹	-2.36172X10 ⁻⁰⁵	3.35364X10 ⁻⁰³
4500	1.56341X10 ⁺⁰¹	1.56252X10 ⁺⁰¹	2.79819X10 ⁺⁰¹	-8.88776X10 ⁻⁰⁵	1.59847X10 ⁻⁰²
5000	1.74207X10 ⁺⁰¹	1.73861X10 ⁺⁰¹	2.79025X10 ⁺⁰¹	-2.49407X10 ⁻⁰⁴	5.53730X10 ⁻⁰²
5500	1.92980X10 ⁺⁰¹	1.91929X10 ⁺⁰¹	2.77070X10 ⁺⁰¹	-5.62535X10 ⁻⁰⁴	1.50958X10 ⁻⁰¹
6000	2.13599X10 ⁺⁰¹	2.10943X10 ⁺⁰¹	2.73080X10 ⁺⁰¹	-1.06559X10 ⁻⁰³	3.39583X10 ⁻⁰¹
6500	2.37445X10 ⁺⁰¹	2.31666X10 ⁺⁰¹	2.66128X10 ⁺⁰¹	-1.73719X10 ⁻⁰³	6.47638X10 ⁻⁰¹
7000	2.66239X10 ⁺⁰¹	2.55164X10 ⁺⁰¹	2.55603X10 ⁺⁰¹	-2.46961X10 ⁻⁰³	1.06330X10 ⁺⁰⁰
7500	3.01760X10 ⁺⁰¹	2.82798X10 ⁺⁰¹	2.41623X10 ⁺⁰¹	-3.08746X10 ⁻⁰³	1.51833X10 ⁺⁰⁰
8000	3.45345X10 ⁺⁰¹	3.16140X10 ⁺⁰¹	2.25204X10 ⁺⁰¹	-3.42318X10 ⁻⁰³	1.90451X10 ⁺⁰⁰
$\log P/P_0 = 0$					

Table XIV (Cont.) Pressure, density derivative of pressure (temperature constant), molecular weight, temperature and density derivatives of molecular weight

$T^{\circ}K$	$\frac{P}{P_c}$	$\frac{\partial P}{\partial P_c}$	M_{gms}	$\frac{\partial M}{\partial T} \frac{gms}{^{\circ}K}$	$\frac{\partial M}{\partial P_c}$
2000	6.94058X10 ⁻⁰¹	6.94058X10 ⁻⁰⁰	2.80140X10 ⁻⁰¹	-2.17866X10 ⁻¹¹	7.68569X10 ⁻¹¹
2500	8.67572X10 ⁻⁰¹	8.67572X10 ⁻⁰⁰	2.80140X10 ⁻⁰¹	-4.01949X10 ⁻⁰⁹	2.21901X10 ⁻⁰⁸
3000	1.04108X10 ⁻⁰²	1.04108X10 ⁻⁰¹	2.80139X10 ⁻⁰¹	-1.20958X10 ⁻⁰⁷	9.63253X10 ⁻⁰⁷
3500	1.21461X10 ⁻⁰²	1.21460X10 ⁻⁰¹	2.80137X10 ⁻⁰¹	-1.30521X10 ⁻⁰⁶	1.41711X10 ⁻⁰⁵
4000	1.38822X10 ⁻⁰²	1.38816X10 ⁻⁰¹	2.80118X10 ⁻⁰¹	-7.47210X10 ⁻⁰⁶	1.06103X10 ⁻⁰⁴
4500	1.56219X10 ⁻⁰²	1.56191X10 ⁻⁰¹	2.80038X10 ⁻⁰¹	-2.81716X10 ⁻⁰⁵	5.06669X10 ⁻⁰⁴
5000	1.73733X10 ⁻⁰²	1.73624X10 ⁻⁰¹	2.79786X10 ⁻⁰¹	-7.95169X10 ⁻⁰⁵	1.76542X10 ⁻⁰³
5500	1.91537X10 ⁻⁰²	1.91202X10 ⁻⁰¹	2.79158X10 ⁻⁰¹	-1.81959X10 ⁻⁰⁴	4.88296X10 ⁻⁰³
6000	2.09934X10 ⁻⁰²	2.09079X10 ⁻⁰¹	2.77848X10 ⁻⁰¹	-3.55145X10 ⁻⁰⁴	1.13178X10 ⁻⁰²
6500	2.29394X10 ⁻⁰²	2.27497X10 ⁻⁰¹	2.75468X10 ⁻⁰¹	-6.10836X10 ⁻⁰⁴	2.27730X10 ⁻⁰²
7000	2.50551X10 ⁻⁰²	2.46796X10 ⁻⁰¹	2.71607X10 ⁻⁰¹	-9.45434X10 ⁻⁰⁴	4.07088X10 ⁻⁰²
7500	2.74187X10 ⁻⁰²	2.67419X10 ⁻⁰¹	2.65921X10 ⁻⁰¹	-1.33472X10 ⁻⁰³	6.56460X10 ⁻⁰²
8000	3.01164X10 ⁻⁰²	2.89909X10 ⁻⁰¹	2.58242X10 ⁻⁰¹	-1.73437X10 ⁻⁰³	9.65113X10 ⁻⁰²

$\log M_c = 1.0$

Table XIV Pressure, density derivative of pressure (temperature constant), molecular weight, temperature and density derivatives of molecular weight

T°K	$C_v \frac{\text{cal}}{\text{gm}^\circ\text{K}}$	$C_p \frac{\text{cal}}{\text{gm}^\circ\text{K}}$	γ	a/a_0
2000	2.35174X10 ⁻⁰¹	3.06083X10 ⁻⁰¹	1.30151X10 ⁺⁰⁰	2.54014X10 ⁺⁰⁰
2500	2.40561X10 ⁻⁰¹	3.11476X10 ⁻⁰¹	1.29478X10 ⁺⁰⁰	2.83262X10 ⁺⁰⁰
3000	2.47138X10 ⁻⁰¹	3.18239X10 ⁻⁰¹	1.28769X10 ⁺⁰⁰	3.09452X10 ⁺⁰⁰
3500	2.82691X10 ⁻⁰¹	3.56038X10 ⁻⁰¹	1.25946X10 ⁺⁰⁰	3.30639X10 ⁺⁰⁰
4000	4.55833X10 ⁻⁰¹	5.43414X10 ⁻⁰¹	1.19213X10 ⁺⁰⁰	3.44454X10 ⁺⁰⁰
4500	1.00845X10 ⁺⁰⁰	1.15945X10 ⁺⁰⁰	1.14973X10 ⁺⁰⁰	3.61342X10 ⁺⁰⁰
5000	2.19377X10 ⁺⁰⁰	2.56902X10 ⁺⁰⁰	1.17104X10 ⁺⁰⁰	3.92812X10 ⁺⁰⁰
5500	3.74183X10 ⁺⁰⁰	4.61513X10 ⁺⁰⁰	1.23338X10 ⁺⁰⁰	4.44211X10 ⁺⁰⁰
6000	4.33229X10 ⁺⁰⁰	5.50299X10 ⁺⁰⁰	1.27022X10 ⁺⁰⁰	5.11084X10 ⁺⁰⁰
6500	3.10729X10 ⁺⁰⁰	3.87081X10 ⁺⁰⁰	1.24571X10 ⁺⁰⁰	5.75509X10 ⁺⁰⁰
7000	1.62615X10 ⁺⁰⁰	1.99768X10 ⁺⁰⁰	1.22847X10 ⁺⁰⁰	6.27582X10 ⁺⁰⁰
7500	9.64916X10 ⁻⁰¹	1.20000X10 ⁺⁰⁰	1.24364X10 ⁺⁰⁰	6.69738X10 ⁺⁰⁰
8000	8.50260X10 ⁻⁰¹	1.05740X10 ⁺⁰⁰	1.24361X10 ⁺⁰⁰	6.98033X10 ⁺⁰⁰

$\log P/P_0 = -3.0$

T°K	$C_v \frac{\text{cal}}{\text{gm}^\circ\text{K}}$	$C_p \frac{\text{cal}}{\text{gm}^\circ\text{K}}$	γ	a/a_0
2000	2.35173X10 ⁻⁰¹	3.06083X10 ⁻⁰¹	1.30152X10 ⁺⁰⁰	2.54014X10 ⁺⁰⁰
2500	2.40483X10 ⁻⁰¹	3.11394X10 ⁻⁰¹	1.29486X10 ⁺⁰⁰	2.83270X10 ⁺⁰⁰
3000	2.44798X10 ⁻⁰¹	3.15768X10 ⁻⁰¹	1.28991X10 ⁺⁰⁰	3.09714X10 ⁺⁰⁰
3500	2.57563X10 ⁻⁰¹	3.29240X10 ⁻⁰¹	1.27828X10 ⁺⁰⁰	3.33044X10 ⁺⁰⁰
4000	3.13792X10 ⁻⁰¹	3.89816X10 ⁻⁰¹	1.24227X10 ⁺⁰⁰	3.51170X10 ⁺⁰⁰
4500	4.95710X10 ⁻⁰¹	5.89443X10 ⁻⁰¹	1.18908X10 ⁺⁰⁰	3.65234X10 ⁺⁰⁰
5000	9.26225X10 ⁻⁰¹	1.07685X10 ⁺⁰⁰	1.16263X10 ⁺⁰⁰	3.83375X10 ⁺⁰⁰
5500	1.69195X10 ⁺⁰⁰	1.99540X10 ⁺⁰⁰	1.17935X10 ⁺⁰⁰	4.11978X10 ⁺⁰⁰
6000	2.67496X10 ⁺⁰⁰	3.28361X10 ⁺⁰⁰	1.22753X10 ⁺⁰⁰	4.54173X10 ⁺⁰⁰
6500	3.40909X10 ⁺⁰⁰	4.34842X10 ⁺⁰⁰	1.27553X10 ⁺⁰⁰	5.09091X10 ⁺⁰⁰
7000	3.32207X10 ⁺⁰⁰	4.27417X10 ⁺⁰⁰	1.28660X10 ⁺⁰⁰	5.69083X10 ⁺⁰⁰
7500	2.47097X10 ⁺⁰⁰	3.12578X10 ⁺⁰⁰	1.26500X10 ⁺⁰⁰	6.24091X10 ⁺⁰⁰
8000	1.58346X10 ⁺⁰⁰	1.97760X10 ⁺⁰⁰	1.24891X10 ⁺⁰⁰	6.70352X10 ⁺⁰⁰

$\log P/P_0 = -2.0$

Table XV Specific heats, specific heat ratio, speed of sound

T°K	$C_v \frac{\text{cal}}{\text{gm} \cdot \text{K}}$	$C_p \frac{\text{cal}}{\text{gm} \cdot \text{K}}$	γ	a/a_0
2000	2.35173X10 ⁻⁰¹	3.06083X10 ⁻⁰¹	1.30152X10 ⁺⁰⁰	2.54014X10 ⁺⁰⁰
2500	2.40458X10 ⁻⁰¹	3.11368X10 ⁻⁰¹	1.29489X10 ⁺⁰⁰	2.83273X10 ⁺⁰⁰
3000	2.44058X10 ⁻⁰¹	3.14986X10 ⁻⁰¹	1.29062X10 ⁺⁰⁰	3.09798X10 ⁺⁰⁰
3500	2.49609X10 ⁻⁰¹	3.20761X10 ⁻⁰¹	1.28505X10 ⁺⁰⁰	3.33906X10 ⁺⁰⁰
4000	2.68532X10 ⁻⁰¹	3.41043X10 ⁻⁰¹	1.27002X10 ⁺⁰⁰	3.54925X10 ⁺⁰⁰
4500	3.27565X10 ⁻⁰¹	4.05416X10 ⁻⁰¹	1.23766X10 ⁺⁰⁰	3.71894X10 ⁺⁰⁰
5000	4.70316X10 ⁻⁰¹	5.64031X10 ⁻⁰¹	1.19925X10 ⁺⁰⁰	3.86749X10 ⁺⁰⁰
5500	7.46458X10 ⁻⁰¹	8.79763X10 ⁻⁰¹	1.17858X10 ⁺⁰⁰	4.04363X10 ⁺⁰⁰
6000	1.18503X10 ⁺⁰⁰	1.40486X10 ⁺⁰⁰	1.18550X10 ⁺⁰⁰	4.28498X10 ⁺⁰⁰
6500	1.75463X10 ⁺⁰⁰	2.13426X10 ⁺⁰⁰	1.21635X10 ⁺⁰⁰	4.61172X10 ⁺⁰⁰
7000	2.32942X10 ⁺⁰⁰	2.93354X10 ⁺⁰⁰	1.25934X10 ⁺⁰⁰	5.02945X10 ⁺⁰⁰
7500	2.70356X10 ⁺⁰⁰	3.50317X10 ⁺⁰⁰	1.29575X10 ⁺⁰⁰	5.52014X10 ⁺⁰⁰
8000	2.69804X10 ⁺⁰⁰	3.53224X10 ⁺⁰⁰	1.30919X10 ⁺⁰⁰	6.03992X10 ⁺⁰⁰

$\log P/P_0 = -1.0$

T°K	$C_v \frac{\text{cal}}{\text{gm} \cdot \text{K}}$	$C_p \frac{\text{cal}}{\text{gm} \cdot \text{K}}$	γ	a/a_0
2000	2.35173X10 ⁻⁰¹	3.06082X10 ⁻⁰¹	1.30152X10 ⁺⁰⁰	2.54014X10 ⁺⁰⁰
2500	2.40451X10 ⁻⁰¹	3.11360X10 ⁻⁰¹	1.29490X10 ⁺⁰⁰	2.83274X10 ⁺⁰⁰
3000	2.43823X10 ⁻⁰¹	3.14739X10 ⁻⁰¹	1.29084X10 ⁺⁰⁰	3.09825X10 ⁺⁰⁰
3500	2.47093X10 ⁻⁰¹	3.18079X10 ⁻⁰¹	1.28728X10 ⁺⁰⁰	3.34190X10 ⁺⁰⁰
4000	2.54185X10 ⁻⁰¹	3.25600X10 ⁻⁰¹	1.28095X10 ⁺⁰⁰	3.56403X10 ⁺⁰⁰
4500	2.73780X10 ⁻⁰¹	3.46857X10 ⁻⁰¹	1.26691X10 ⁺⁰⁰	3.76030X10 ⁺⁰⁰
5000	3.20251X10 ⁻⁰¹	3.98104X10 ⁻⁰¹	1.24309X10 ⁺⁰⁰	3.92907X10 ⁺⁰⁰
5500	4.11803X10 ⁻⁰¹	5.00889X10 ⁻⁰¹	1.21633X10 ⁺⁰⁰	4.08349X10 ⁺⁰⁰
6000	5.65941X10 ⁻⁰¹	6.78128X10 ⁻⁰¹	1.19823X10 ⁺⁰⁰	4.24902X10 ⁺⁰⁰
6500	7.92870X10 ⁻⁰¹	9.48069X10 ⁻⁰¹	1.19574X10 ⁺⁰⁰	4.44822X10 ⁺⁰⁰
7000	1.08785X10 ⁺⁰⁰	1.31573X10 ⁺⁰⁰	1.20946X10 ⁺⁰⁰	4.69507X10 ⁺⁰⁰
7500	1.42477X10 ⁺⁰⁰	1.76121X10 ⁺⁰⁰	1.23613X10 ⁺⁰⁰	4.99698X10 ⁺⁰⁰
8000	1.75445X10 ⁺⁰⁰	2.22763X10 ⁺⁰⁰	1.26970X10 ⁺⁰⁰	5.35460X10 ⁺⁰⁰

$\log P/P_0 = 0$

Table XV (Cont.) Specific heats, specific heat ratio, speed of sound

T°K	$C_v \frac{\text{cal}}{\text{gm}^\circ\text{K}}$	$C_p \frac{\text{cal}}{\text{gm}^\circ\text{K}}$	γ	a/a_0
2000	2.35173X10 ⁻⁰¹	3.06082X10 ⁻⁰¹	1.30152X10 ⁺⁰⁰	2.54014X10 ⁺⁰⁰
2500	2.40448X10 ⁻⁰¹	3.11358X10 ⁻⁰¹	1.29490X10 ⁺⁰⁰	2.83274X10 ⁺⁰⁰
3000	2.43749X10 ⁻⁰¹	3.14661X10 ⁻⁰¹	1.29091X10 ⁺⁰⁰	3.09833X10 ⁺⁰⁰
3500	2.46297X10 ⁻⁰¹	3.17231X10 ⁻⁰¹	1.28800X10 ⁺⁰⁰	3.34281X10 ⁺⁰⁰
4000	2.49645X10 ⁻⁰¹	3.20714X10 ⁻⁰¹	1.28467X10 ⁺⁰⁰	3.56906X10 ⁺⁰⁰
4500	2.56711X10 ⁻⁰¹	3.28302X10 ⁻⁰¹	1.27888X10 ⁺⁰⁰	3.77728X10 ⁺⁰⁰
5000	2.72193X10 ⁻⁰¹	3.45271X10 ⁻⁰¹	1.26847X10 ⁺⁰⁰	3.96626X10 ⁺⁰⁰
5500	3.02191X10 ⁻⁰¹	3.78677X10 ⁻⁰¹	1.25310X10 ⁺⁰⁰	4.13691X10 ⁺⁰⁰
6000	3.53225X10 ⁻⁰¹	4.36445X10 ⁻⁰¹	1.23560X10 ⁺⁰⁰	4.29566X10 ⁺⁰⁰
6500	4.30999X10 ⁻⁰¹	5.26184X10 ⁻⁰¹	1.22084X10 ⁺⁰⁰	4.45404X10 ⁺⁰⁰
7000	5.39094X10 ⁻⁰¹	6.53936X10 ⁻⁰¹	1.21302X10 ⁺⁰⁰	4.62424X10 ⁺⁰⁰
7500	6.77698X10 ⁻⁰¹	8.22808X10 ⁻⁰¹	1.21412X10 ⁺⁰⁰	4.81574X10 ⁺⁰⁰
8000	8.42574X10 ⁻⁰¹	1.03141X10 ⁺⁰⁰	1.22412X10 ⁺⁰⁰	5.03478X10 ⁺⁰⁰

$\log P/P_0 = 1.0$

Table XV (Cont.) Specific heats, specific heat ratio, speed of sound